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measured by several methods. This research attempted to determine occupational exposure from the amount of contaminant deposited on respirator cartridges. The flowrate through the respirator was estimated by existing ergonomic and respiratory ventilation models. The respirator concentrations were compared with simultaneous breathing zone air samples. A respiration flow model was modified into 18 different variations depending on 1) the increase in oxygen required per increase in workload; 2) estimate of total ergonomic workload; and 3) the basal metabolic rate. / Models were rejected if the required flowrate of oxygen exceeded the calculated maximum possible flowrate. Seven dust/mist samples and five organic vapor samples were taken during sanding and spray painting operations. the 18 models only 5 were acceptable. Dust/mist respirator results were 1.5 to 2.2 times less than the breathing zone samples., No significant difference was found between 1 average and 5 minimum flowrate respirator models for dust/mist samples. / Respirator cartridge organic vapor constituents were 1.0 to 2.5 times less than the charcoal tube values. Four of the organic vapor samples and 3 of 5 individual constituents were not significantly different. models appear to overestimate the actual flow, although factors such as mask leakage, faceshield blocking, sonsitivity of filter pads to relative humidity, and differences in analytical sensitivities made quantitative conclusions unreliable. The results of organic vapor respirator cartridges did show countenance for this procedure in screening workplace exposures or estimating a respirator workplace protection factor. Regardy filter Analysis, Respirator, (SDW) -

Analysis of Air Purifying Respirator Cartridges and Filters as a Determination of Occupational Exposure

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Introduction:

A worker's exposure to airborne workplace contaminants can be measured by several methods. As air sampling equipment technology has improved, personal sampling increasingly relies upon battery operated pumps or passive dosimeters. However, breathing zone samples do not evaluate the effectiveness of respiratory protection in areas requiring personal protective equipment to supplement traditional engineering controls. Furthermore, breathing zone sample results can vary by the type (passive vs. active), location and orientation of the collecting device.

In an article published in 1988, First [1] stated "Analysis of the respirator pad or chemical cartridge gives a good integrated sample of the air that would have reached the lungs, although the exact air volume can only be estimated." This research attempted to determine industrial airborne workplace concentrations based on the amount of contaminant deposited on respirator cartridges. The airborne concentrations were calculated by estimating the flowrate through the respirator with existing ergonomic and human ventilatory models. The calculated concentrations were compared with concurrent continuous breathing zone air samples to determine any statistical correlation. The goal of this research was to determine if the respirator cartridge analysis method could be used as a screening device for estimating workplace airborne concentrations.

Background:

The use of respirator pads to determine exposure to pesticides was described by Durham and Wolf [2] in 1962. Respiratory exposure was estimated by the amount of pesticide deposited on the filter pads of a properly fitted "single unit respirator and a modified plastic funnel" covering. The covering protected the respirator pad from direct spray. The stem of the funnel covering was plugged and two 12mm holes drilled 6mm apart midway between the base and the apex. During sampling, the holes were directed downward to simulate the aerodynamic effect of human nostrils. Durham and Wolf listed several previous studies comparing the results of respirator pad analysis to breathing zone air samples.

Measurements by Batchelor & Walker [3] during orchard spraying with parithion indicated the respiratory pad technique gave values 3 to 5 times greater (in mg/kg/day) than air sampling results. Durham and Wolfe [2] contended that the ratios of respiratory pad samples to air sampling results were actually "of the same order of magnitude" because Batchelor & Walker did not shield the respirator pads to prevent impingement of the parithion aerosol. Durham and Wolfe argued that about 75% of the apparent exposure on an unshielded respirator pad was actually due to impingement and therefore not representative of potential inhalable contaminates.

Further measurements of DDT by Wolfe [4] revealed the respirator pad method gave values about two times as high as breathing zone samples. Again, the author stated the results were "considered to be about the same order of magnitude."

This method continues to be utilized in agricultural pesticide sampling, e.g. see Winterlin, et. al [5] in a 1984 survey of strawberry harvesters in California. Winterlin's 28 liter per minute (lpm) "low flow" breathing zone results for captan and THPI (tetrahydrophtalimide) were 2 to 5 times the respirator pad values [assuming 10 lpm respiration rate as stated by the author; in micrograms per cubic meter].

The results of these studies question the validity of correlating respirator filter sampling to breathing zone air sampling. However, all of the above cited studies assumed a single worker breathing rate over the entire sampling period (8 lpm for Batchelor, et. al. [3] and Wolfe [4] versus 10 lpm for Winterlin, et al. [5]). This assumption was not well-founded if the workers used multiple body positions (i.e. sitting, standing, or walking) during the operation. It was also not logical if the physical workload varied during the sampling period. Using improvements in estimating the exact respiratory air volume of a worker, it was anticipated that the respirator filter cartridge analysis method would approximate the continuous breathing zone air sampling pump results.

Sampling Methods:

Sampling Location and Operations: Sampling was conducted at three separate industrial areas at Pope Air Force Base located in Fayatteville, North Carolina. The first area was a vehicle maintenance facility. Work at this facility included body work and spray painting on military cars, vans, and specialized vehicles. All spray painting was conducted in an enclosed auto spray paint booth. The paint booth ventilation system provided an average exhaust ventialtion of 212 cubic feet per minute per square foot of cross section (CFM/Ft²). This facility was used for sampling painting operations for paint mist and organic vapors. Personnel used an air atomization method of spraying to apply a mixture of acrylic enamel, thinner and hardener (drier).

The second industrial area studied was an aircraft structual repair shop used for sanding and painting specialized military equipment such as aircraft engine housings and maintenance scaffolding. Operations were conducted in a waterfall paint booth which provided an average exhaust ventilation of 143.3 CFM/Ft². This facility was used for sampling sanding operations only. Sanding operations utilized a pneumatic orbital disk sander.

The last industrial area was a fiberglass repair shop. The personnel in this shop mended and sanded aircraft components. The shop included two large paint booths with exhaust flow rates of 505 CFM/Ft^2 and 488 CFM/Ft^2 . One sanding operation was sampled from

this shop. During this study personnel used a pneumatic orbital disk sander similar to that used in the sanding operations above.

The personnel in all areas wore cartridge-type respirators and were previously monitored through industrial hygiene and respiratory protection programs. The respirators worn during painting were half-face dual filter (American Optical) with organic vapor cartridges (R51A TC-23C-235) and dust/mist prefilter (R30 TC21C-144). The dust/mist filters were constructed of resin coated composite fibers. During sanding operations the same model of repirator was worn, but only the dust/mist filter was used.

Sampling Techniques & Analysis: Painting and sanding operations were sampled for total dust and mist particulates. Breathing zone dust samples were taken with 35 millimeter mixed cellulose ester filters (0.8 micrometer; matched weight) in an open face cassette. The sampling pumps (DuPont Alpha 1) were calibrated to a flowrate of 2.0 liters per minute (lpm). During sampling, the cassette filter was placed in the breathing zone of the subject by attachment to the coverall collar. The filter cassette was attached such that the filter was vertical (perpendicular to the floor) with the open face directed towards the front of a standing worker. The respirator samples were collected by installing new dust/mist filters over each respirator cartridge. The filters were attached over the organic vapor cartridges for painting operations. During sanding operations, the organic vapor cartridges were removed and the filters attached directly to the respirator. Both the membrane

and respirator filters were analyzed by determining the pre-sampling versus post-sampling weight changes utilizing an analytical balance (Mettler 52L).

Initial sampling revealed the weight of the respirator filters were influenced by the relative humidity and the elapsed time at ambient laboratory conditions. Repeated weighting, over elapsed time, showed that the weight of a resin coated respirator filter changed over time until an equilibrium weight was achieved. The filter weight continued to change until elapsed time reached two hours. A plot of percent of total filter weight change (during elapsed time of two hours) versus elapsed time at ambient laboratory conditions revealed an inverse exponential curve (Figure 1). This figure indicated that 95% of the total weight gain/loss occurred within 1.5 hours. Therefore, all samples (pre-weight and post-weight) were analyzed after 1.5 hours of equilibration to ambient laboratory conditions.

In addition, four (4) blank respirator filters were repeatedly weighted over a period of several weeks at relative humidities ranging from 50% to 70%. Thirteen (13) sets of measurements were taken at eight (8) different relative humidities. A regression curve was calculated from these measurements to estimate the average percent change in filter weight versus relative humidity (Figure 2). The regression indicated that the percent change in respirator filter weight is determined by the relative humidity with the following equation:

Figure 1: % Filter Wt Change vs. Time

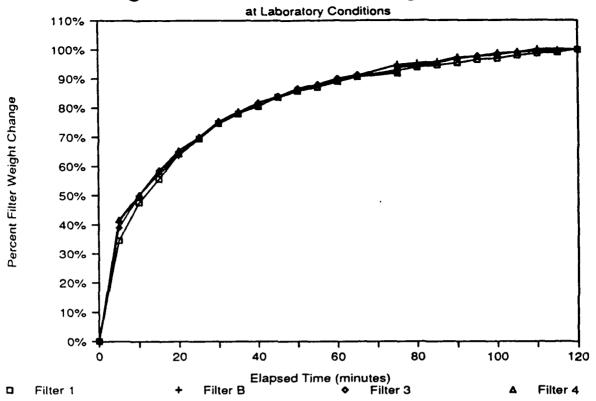
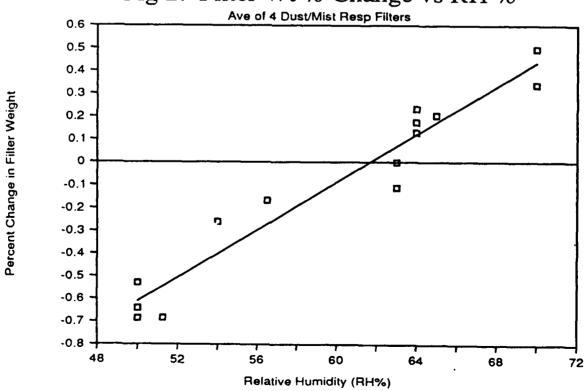


Fig 2: Filter Wt % Change vs RH %



The percent change in filter weight is relatively small (-0.7% to +0.5%) with respect to changes in relative humidity. However, it corresponds to corrections of up to 2.5 times the sample weight (Table 1). This is explained by the fact that the sample weights (2.1 mg to 27.1 mg) were only an average of 0.6 percent of the respirator filter weights (2296.18 mg to 2664.24 mg). The regression analysis was used to correct all respirator filter sampling results.

Three painting operations were sampled for detectable aromatic hydrocarbons. A list of analyzed hydrocarbons can be found in Table 2. The breathing zone samples of painting operations were obtained with large charcoal tubes (1 gram front portion, 0.25 grams rear portion) at a flow rate of 1.0 lpm. New organic vapor respirator cartridges were used for each sample. After each sample the charcoal tube was capped and respirator cartridges wrapped in foil. All samples were transported on ice to the laboratory, where they remained until analyzed. All organic vapor samples were analyzed on a Perkin Elmer 990 gas chromatograph and analyzer. Desorption efficiencies and blank analysis were determined for both the charcoal tube and respirator cartridge. The average weight of several blank organic vapor cartridges was approximately 52 grams of activated charcoal.

Table 1. Corrections to Dust/Mist Samples
Due to Changes in Laboratory Relative Humidity

Sample #	Uncorrected Resp Filter Sample Wt (mg)	Change to Samp Wt due to RH% (mg)	
1 Left Filter		-6.39	0.30
1 Right Filte	r 18.15	-6.39	0.35
2 Left Filter	13.29	-6.83	0.51
2 Right Filte	r 11.0	-6.83	0.62
3 Left Filter	5.87	+2.78	0.47
3 Right Filte	r 3.35	+2.78	0.83
4 Left Filter	8.35	-4.75	0.57
4 Right Filte	r 2.10	-5.17	2.46*
5 Left Filter	5.13	-1.88	0.37
5 Right Filte	r 9.65	-1.68	0.17
6 Left Filter	27.64	-1.75	0.06
6 Right Filte	r 21.13	-1.73	0.08
7 Left Filter	26.97	-1.81	0.07
7 Right Filte		-1.86	0.07

Respirator filter weights without samples ranged from: 2296.18 mg to 2664.24 mg

<u>Average sample wt = 14.38 mg</u> = 0.0058 ~= 0.6% Average filter wt = 2480.0 mg

Table 2. Volatile Aromatic Hydrocarbons Analyzed
During Painting Operations

Ethlyene Dichloride	n-Octane
n-Heptane	Toluene
Isopropanol	1,1,1-Trichloroethane
Methyl Ethyl Ketone	Trichloroethlyene
Methycyclohexane	m-Xylene
Methycyclopentane	o-Xylene
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^{*} Note: Sample weight taken as zero.

The respirator cartridges were removed from the freezer, immediately opened, and the charcoal transfered into a 500 ml beaker. The charcoal was thoroughly agitated for one minute. Then five one-gram samples (ten for organic vapor samples #4 and #5) were selected from the beaker. The beaker was agitated between each sample. The samples were weighted in Miniert screw cap reaction vials to +/- .0005 grams. The results of the five (or ten) grab samples were averaged for each chemical constituent and multiplied by 52.

The respirator and breathing zone results were compared by mass collected per volume of air sampled. This concentration was calculated by dividing the measured mass collected on the filters by the volume of air that flowed through the respirator or sampling pump. The volume of air flowing through the sampling pump was determined by multiplying the average flowrate (pre-operation calibration and post-operation calibration) by the pump operating time. The respirator volumetric flowrate was calculated by a model adapted from predictions of human respiration during exercise.

Respirator Airflow Estimates:

Previous respirator pad studies [2, 3, 4, 5] have shown that the assumption of constant worker respiration over the sampling period leads to inconsistent results. This research determined the amount of air flowing through the respirator filters by a predictive

human respiration model adapted from Hansen, et al [6]. Hansen's study predicted a range of expected breathing performance in normal subjects during exercise. Measurements of the rate of oxygen uptake (Vol Rate O_2 ; lpm) and expired minute ventilation (Vol Rate Exp; lpm) found different predictive ratios of Vol Rate Exp/Vol Rate O_2 at progressive stages of exercise (Table 3).

Table 3. Predictive Ratios of Expired Minute Volume to Rate of Oxygen Uptake at Progessive Levels of Exercise*

Vol Rate Expired (BPTS) / Vol Rate 0₂ Required =

```
= 32.2 +/- 12.1 (At Rest)

" = 28.5 +/- 8.1 (At 0 Watts)

" = 26.5 +/- 4.4 (At AT**)

" = 37.7 +/- 6.9 (At Maximum Exercise)
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** AT = Aerobic Threshold of Oxygen Required or Consumed = $0.56 \times Maximum Vol Rate O_2 Required$

```
Vol Rate O_2 (max) = [Weight(kg) x (50.75 - 0.372 x Age(yrs))]
* From Hansen, et. al. [6]
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The ratios are necessary because it is impossible to predict with any degree of accuracy the volume of air expired during exercise. However, it is possible to predict the volumetric rate of oxygen uptake with quite good precision [7]. From Hansen's research, the rate of oxygen uptake with no workload was predicted by the equation: Vol Rate O_2 (0 Watts) = 5.89 x W + 140, where W is the subject's body weight in kilograms. A worker's maximum possible volumetric rate of oxygen uptake was also predicted by the equation: Vol Rate O_2 (max) = W x (50.72 - 0.372 x A), where A is the worker's

age in years. From these predictions, Hansen et. al. could determine a worker's total volume of expired (or inspired) air, if the total rate of oxygen required during the task is known.

The rates of oxygen required during the sampled operations were calculated in three steps. The first step was to estimate the total work rate (power) necessary for the worker to perform the operation. The second step was to subtract the worker's basal metabolic rate from the total work rate to determine the actual physical work rate of the operation. The final step was to calculate the worker's increase in the rate of oxygen required due to task. Then this increase was added to the rate of oxygen required at zero work rate (0 watts). This yielded a total rate of oxygen required (lpm) per work rate (watt) for the operation.

Ergonomic Estimates of Total Energy Required: An estimate of the operation work rate was determined from three (3) ergonomic references. Krager and Hancock [8] list work rates for average workers at specific operations. For this research, using Krager and Hancock's list, both sanding and painting require a total work rate of 3400 calories per minute. Passmore and Durnin [9] also list work rates for average workers at specific operations. Both sanding and painting require 2000 calories per minute using Passmore and Durnin's list. Salvendy [10] does not list work rates by specific operations, but uses estimates based on a worker's position and movement. A copy of Salvendy's values are listed in Table 4. All of these work rates are tabulated for a standardized man of 70

kilograms weight, 175 cm height and 30 years old.

Table 4. Estimated Energy Expenditure*

Position of Worker (A) Sitting	Net Energy Expended (kcal/min) 0.3
Kneeling	0.5
Crouching	0.5
Standing	0.6
Stooping	0.8
Type of Work (B)	Net Energy Expended (kcal/min)
One Arm Work	Light 0.7 - 1.2
11	Medium 1.2 - 1.7
II	Heavy 1.7 - 2.2
Both Arms Work	Light 1.5 - 2.0
n	Medium 2.0 - 2.5
11	Heavy 2.5 - 3.0

Estimated Energy Expenditure (kcal/min) = A + B Note: 1.0 kcal/min = 69.735 Watts * From Salvendy, Table 3.5.4 [10]

Basal Metabolic Rate: Ergonomic estimates provide the total power (work rate) required for a person to perform an operation [8,9]. The worker's basal metabolic rate must be subtracted from the total energy to determine the actual physical work rate. In living organisms the total power required for any activity is the sum of that power necessary for the organism to sustain basic metabolism at rest (basal metabolic rate) plus the power required to perform the activity (physical work rate). Therefore, the actual rate of physical work for any operation is the estimated ergonomic rate minus the basal metabolic rate. In this research the basal metabolic rate was determined by three methods:

- 1) Calculate the rate of oxygen required at rest as follows: Vol Rate O_2 (rest;ml/min.) = Vol Rate O_2 (0 Watts) = (5.89 x Weight (kg)) + 140 [6]. The power required at rest was then calculated from the inverse of 9.3 (+/- 1.35) milliliters of oxygen per minute required per watt required [6].
- 2) Calculate the rate of oxygen required at rest as follows: Vol Rate O_2 (rest;ml/min.) = Vol Rate O_2 (0 Watts) = (5.89 x Weight (kg)) + 140 [6]. The rate of energy required at rest was then calculated from the inverse of 11.5 milliliters of oxygen per minute required or consumed per watt required [11].
- 3) From a table of standard values for calories per hour per square meter of body surface area at various ages by sex [12]. These values are listed in Table 5. The body surface area was calculated as follows: Surface Area $(m^2) = 0.007184 \times (Weight (kg))^{0.425} \times (Height (cm))^{0.725}$.

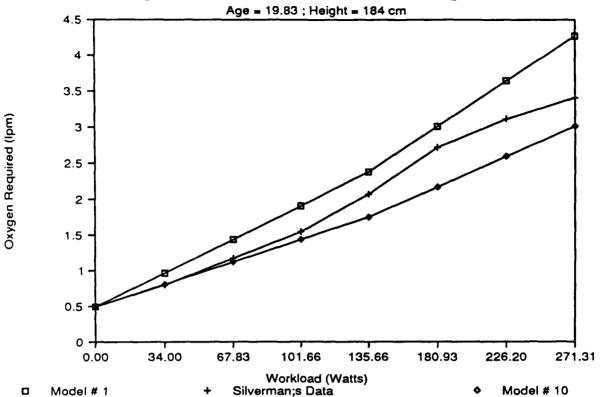
Table 5: Basal Metabolic Rate in Calories per Square Meter of Body Surface Area per Hour at Various Ages as of Last Birthday*

List	ing for Males		_
Age Last Birthda	y Mean	Value	$(Cal/m^2/hr)$
19	-	42.32	
19.5		42.00	
20 - 21		41.43	
22 - 23		40.82	
24 - 27		40.24	
28 - 29		39.81	
30 - 34		39.34	
35 - 39		38.68	
40 - 44		38.00	
45 - 49		37.37	
50 - 54		36.73	
* From Boothby,	et. al. Table	4 [11]	•

Volumetric Rate of Oxygen Required Per Work Rate: With the actual physical rate known, the total rate of oxygen required per work rate was calculated from the rate of oxygen required at no work (O Watts; see equation above) plus the increase in rate of oxygen uptake caused by the physical work rate. The increase in Vol Rate O₂ required per increase in work rate was determined from two (2) references. Hansen's [6] model assumed an increase of 9.3 (+/-1.35) milliliters of oxygen per minute per increased watt of physical work rate (0.0093 lpm/watt). The Handbook of Respiration [11] assumed an increase of 13.94 milliliters of oxygen per minute per increased watt of physical work rate (0.01394 lpm/watt). Consequently, a worker's volumetric rate of oxygen (lpm of 02), strictly due to the task, will be the power required by the task (watts) multiplied by the increase in Vol Rate 0, per increase in work rate (lpm/watt). Finally, a worker's total volumetric rate of oxygen was calculated as the sum of the Vol Rate 0, (0 Watts) plus the Vol Rate O_2 strictly due to the operation. To validate the calculation of total Vol Rate O2 required during a task, these models were compared with published clinical data on ventilation rates with respiratory resistance at various workloads [13]. The models demonstrate excellent agreement as shown in Figure 3.

Total Volume of Air Expired: From the calculated total rate of oxygen required and the predicted ratios of Vol Rate Exp/Vol Rate $^{0}2$, the total volume of expired air was computed by knowing the duration of the task. Total volume of expired air = Total volumetric rate of oxygen X Vol rate expired/Vol rate $^{0}2$ X time of operation.

Figure 3: Workload vs. O2 Required



Combining these references and steps yielded eighteen (18) different models to estimate a worker's volume of air through a respirator. For this research it was assumed that the total expired volume equals the total inspired volume, even though the volume of inspired air is slightly larger than the volume expired [14]. This assumption was necessary because the volume of air through the respirator filter (or cartridge) will only include inspired air.

Another assumption was that no face seal leakage occurred during inhalation and therefore there was no penetration of the contaminant through the filter. Lastly, it should also be noted that none of these models consider increased worker breathing due to

the resistance of increased respirator filter load. For the simplicity of the models and the short sampling times involved (maximum length was 2 hours), it was assumed that these factors were negligible.

Results and Discussion:

Operations sampled: There were seven dust/mist samples collected: four samples during sanding on painted metal, one sample while sanding on unpainted fiberglass, and two from spray painting procedures. In addition there were five organic vapor samples carried out during the spray painting operations. The subjects sampled were all males with ages ranging from 21 to 50 years (average = 26.3 years; standard deviation = 8.08 years). lengths of operations sampled ranged from 20 to 120 minutes (average = 54.67 min; S.D. = 26.84 min). The seven dust/mist samples included four different individuals. The four sanding samples (#1, #2, #6, and #7) were all from the same person. The five organic vapor samples included three different individuals two of which were also included in the dust/mist samples (OV-#3 in dust/mist #3; OV-4 and OV-5 in dust/mist #4). In total, over the twelve samples, five (5) different individuals participated in the sampling. During all operations, except organic vapor samples #1 and #2, the respirators were worn during the entire breathing zone sampling period. During dust/mist samples #1, #2, #6 and #7, the subject also wore a full faceshield which partially blocked the respirator filters.

Observations of Operations: The sanding operations involved standing, sitting, stooping and kneeling, while the painting operations only involved standing and stooping (Appendix I). During organic vapor samples #1 and #2, the subject's respirator was removed each time the paint spray gun was refilled. However, the charcoal tube sampling pump was not shut off during refilling.

Refilling the spray paint gun was accomplished outside the paint spray booth on a table adjacent to a large open overhead doorway. The subject poured a mixture of paint, thinner and hardener into the paint spray-gun receptable and agitated the mixture with a stick. The refilling operation lasted from 2 to 12 minutes. The paint spray gun would operate from 10 to 24 minutes between refills. For organic vapor sample #1, the paint spray gun was refilled seven (7) times for a total of 38 minutes. Organic vapor sample # 2 included four (4) refills for a total of 20 minutes. During the remaining organic vapor samples the worker was asked wear the respirator during paint spray gun refills.

General Trends of Raw Data: The weights of dust/mist sampling and organic vapor sampling may be found in Appendix II. Breathing zone samples during sanding operations measured from 0.47 to 5.29 milligrams (mg) of dust, while the respirator filters measured from 10.63 to 50.46 mg. The painting operations breathing zone mist samples ranged from 0.63 to 1.12 mg, while the respirator filters measured from 3.60 to 4.19 mg. There was no observable trend over the seven (7) samples between the ratio of respirator cartridge

sample weight to breathing zone membrane filter sample weight. The ratios of the weights ranged from 3.7 to 25.3 and did not correspond to the length of sampling time.

Weight corrections for respirator filter pads by relative humidity ranged from -6.83 to +2.42 mg (Table 1). Weight corrections were not applied to the breathing zone dust/mist samples. In sample #4, the right cartridge respirator pad had a negative sample value when the weight correction was applied. In this case the sample value taken as 0 mg and the left respirator cartridge filter weight used for the total weight.

For all organic vapor samples the respirator cartridges measured more mass per constituent than the charcoal filter tube. There were no observable trends for the ratios of respirator cartridge constituent mass to charcoal tube constituent mass among or between samples (Table 6). However, for seven (7) constituents, 1,1,1-trichloroethane in OV Sample #1 (OV-1); isopropanol in OV Sample #2 (OV-2); m-xylene in OV Sample #3 (OV-3); isopentane, n-octane, and isopropanol in OV Sample #4 (OV-4); and n-hexane in OV Sample #5 (OV-5), the constituent was detected in the charcoal tube, but not in the respirator cartridges (first case). Three (3) constituents; methyl ethyl ketone and 1,1,1-trichloroethane in OV-3; and 1,1,1-trichloroethane in OV-5, were detected in the respirator cartridges, but not in the charcoal tube (second case). (See Appendix II).

Table 6: Ratios of Charcoal Tube to Respirator Organic Vapor Cartridge Sampling Results

Chemical	Samp # OU-1 BZ / Resp mg / mg	Samp # OU-2 BZ / Resp mg / mg	Samp # 00-3 BZ / Resp mg / mg	Samp # QU-4 BZ / Resp mg / mg	Samp # (JU~5 BZ / Resp mg / mg
Nethyl cyclopentane	0.07	0.09	0.05	0.05	0.05
n-Heptane Curlobeyane	60.0	0.10	0.03	00.0	•
	, c	900	000	0	
engrederonaxana	0.0	90.0	60.03	, ,	
n-Uctane	ი. სა				6.03 0.03
Methyl Ethyl Ketone	0.16	0.0	0.00		0,04
I sepropano I			0.06		0.01
Trichloroethylene	0.02	0.08	0.03		0.05
Toluene	0.02	0.05	0.05	0.06	0.04
Ethlyene Dichloride	0,10	0.09	0.15		0.06
p-Xylene	0.02	90.0	0.04	0.06	0.04
a-Xylene	0.05	0.05	-		0.04
o-Xylene	90.0	0.05	0.04	0.08	0.03
1					
					Samp # 0U-5
Model #17	8Z / Resp	BZ / Resp	BZ / Resp	82 / Resp	BZ / Resp
used for resp vol	/ Cvm/6m	/ E~m/6m	/ E/m/6w	mg/m^3 /	/ E/w/6w
	E^m/6m	6	E^m/gm	E/m/6m	E^m/gm
Chemical	(note 1)	(note 2)			
Methylcyclopentane	1.00	2.01	1.88	1.74	1.29
n-Heptane	1.19	2.37	2.41	2.19	1.18
Cyc. I ohexane	0,22				
Methyl cyclohexane	0.67	1.40	1.56	1.34	
ri-Octane	0.75	1.51			1.18
Methyl Ethyl Ketone	2.27	1.64	0.00		1.32
[scpropano]			2,99		0.19
Trichloroethylene	0.99	2.02	1.49		1.60
Toluene	0.99	1.78	2.55	2.16	•
Ethlyene Dichloride	1.44	2.24	•		2.01
FXylene	0.92	1.39	2.17	2.34	1.35
rıXy1ene	0,75	1.16			1.28
ci-Xylene	0.81	1.13	1.79	2.80	•

Note 1: BZ result includes 38 minutes during refilling when respirator not worn. Note 2: BZ result includes 20 minutes during refilling when respirator not worn.

The detection of some constituents in one method and not the other were probably caused by two different events. In the first case, the detection of constituents in the charcoal tube, but not in the respirator cartridge was probably caused by the greater analytical sensitivity of the charcoal tube. The constituents were detected in relatively low quantities in the charcoal tubes and thus may have been present in the respirator cartridges, but below detectable limits. The analytical detection limit of the respirator cartridges was over ten times (10x) higher (i.e. less sensitive) than the charcoal tubes. This was a consequence of the application of grab sampling from the total weights of charcoal in the respirator filter cartridges. In the charcoal tubes, the entire samples of activated charcoal were analyzed.

In the second case constituents were detected in the respirator cartridge but not in the charcoal tube. This was probably caused by contamination of the respirator cartridge samples. In both samples where this event occurred (OV-3 and OV-5) the respirator cartridges were stored in the laboratory the longest amount of time before analysis (up to 30 days). In addition, the constituents were detected in fairly low concentrations and with very poor precision. In two cases, methyl ethyl ketone in OV-3 and 1,1,1-trichloroethane in OV-5, the precision was so inadequate that the standard deviation of the analysis was greater than the actual amount detected.

Respirator Air Flow Models: The volume of air sampled through a worker's respirator was calculated from a model developed by

Hansen, et al, [6] and modified with respect to increased rate of oxygen required per increase in work rate (lpm/watt); the total work rate required for the operation (watts); and basal metabolic rate (watts). All 18 models were applied to each of the seven dust/mist samples (see Appendix III). Models were rejected if the required total volumetric rate of oxygen (lpm) for the operation exceed the subject's calculated maximum possible volumetric rate of oxygen. For models that calculated total work rate required based on the worker's position (i.e. standing, walking; models #4, #5, #6, #13, #13, and #15), any model was rejected even if only one subject position in one sample met this criteria. Of the 18 models only five (5) were acceptable for all the dust/mist samples. The acceptable models are annotated in Table 7.

To determine if the accepted models provided legitimate estimates of total inspired volume, the calculated rates of expiration were compared to published ventilatory patterns measured during exercise [5]. Published studies measured expired minute volumes of 20.0 (+/- 5.5) lpm up to 93.3 (+/- 23.0) lpm at various stages of exercise. The acceptable respirator air flow models from this research calculated an average expiration rate of 56.3, 46.4, 43.0, 37.0, and 55.0 lpm for models #8, #13, #16, #17, and #18, respectively. All of the models fall within a range of expiration rates that would indicate a moderate level of exercise, which was expected from operations such as sanding and painting.

Table 7: Acceptable Dust/Mist Sample Models

Model Number		Sample Subject Exceed Maximum	Sample #(s)Where Maximum O ₂ Flow
		Oxygen Flowrate	Is Exceeded
1	V11-E8-R11	YES	1,2,3,4,5,6,7
2	V11-E8-R6	YES	1,2,3,4,5,6,7
3	V11-E8-R12	YES	1,2,3,4,5,6,7
4	V11-E10-R11	YES	5
5	V11-E10-R6	YES	5
6	V11-E10-R12	YES	1,2, 5,6,7
7	V11-E9-R11	YES	5
8	V11-E9-R6	NO	none
9	V11-E9-R12	YES	5
10	V6-E8-R11	YES	5
11	V6-E8-R6	YES	5
12	V6-E8-R12	YES	1,2, 4,5, 7
13	V6-E10-R11	NO	none
14	V6-E10-R6	YES	5
15	V6-E10-R12	YES	1,2, 5,6,7
16	V6-E9-R11	NO	none
17	V6-E9-R6	NO	none
18	V6-E9-R12	NO	none

Model Codes:

```
Increased Volume Rate Oxygen Required Per
Increase in Actual Physical Work Rate:
```

Vol Rate 0_2 (0 Watts) = (5.89*Wt(kg)+140)/1000 [lpm]

V11-XX-XX = From Reference 11: 0.01394 lpm 02 required/watt

V6-XX-XX = From Reference 6: 0.0093 lpm O₂ required/watt

Ergonomic Estimate of Total Energy Required:

XX-E8-XX = From Reference 8: 3400 cal/min (238 Watts)

XX-E10-XX = From Reference 10: see Table 4.

XX-E9-XX = From Reference 9: 2000 cal/min (140 Watts)

Basal Metabolic Rate:

Vol Rate O2 (rest) = Vol Rate O_2 (O Watts) [lpm] XX-XX-R11 = From Reference 11: 71.74 watt/lpm O2 rest

XX-XX-R6 = From Reference 6: 107.53 watt/lpm 02 rest

XX-XX-R12 = From Reference 12: see Table 5.

Particle Sizing of Dust/Mist Samples: Particle sizing was conducted to distinguish discrepancies between initial sanding and painting sampling results. By comparing particle sizes with published data, it was possible to determined if the operations were representative of typical industrial processes. During dust/mist samples #2 (sanding) and #3 (painting), 5 and 10 minute samples were obtained for particle sizing. The samples were taken in the breathing zone of the subject during the operation with a membrane filter cassette (0.8 um matched weight). The sampling pump was calibrated to 2.0 lpm. The samples were optically sized with a porton graticule (Ernst Leitz Wetzler Binocular Microscope; 12.5x eyepiece, 10x object). The porton graticule was calibrated with a stage micrometer. The corresponding diameters of the porton numbers were determined by linear regression (Appendix V).

The results of sizing the 5 and 10 minute spray painting samples were identical. A count of 9 fields in each sample measured particle sizes ranging from 0.716 to 16.84 micrometers. The count median aerodymanic diameters (CMAD) were 0.716 microns and the mass median aerodynamic diameters (MMAD) were 5.44 microns. This result agrees with the results by Chan, et al. [15] who measured MMAD of 4.7 - 6.6 microns for conventional air-atomized paint spray guns.

Likewise, the results of the 5 and 10 minute sanding samples were identical. A count of 9 fields in each sample measured particle diameters from 3.74 to 76.0 microns, with a CMAD of 7.934 microns and MMAD of 52.1 microns. The approximate 10 fold increase

in MMAD for sanding versus painting is anticipated because of the abrasive method in which particulates were generated during sanding.

Trends of Calculated Data for Dust/Mist Samples: For all of the acceptable models, the dust/mist breathing zone results were 1.5 to 2.2 times the respirator filter samples (See Appendix III). Respirator flowrate models #13 and #18 determined the respirator concentrations for all dust/mist operations less than the comparable breathing zone results. Only in samples #1 and #2 (sanding operations) with respirator flowrate models #8, #16 and #17 did the respirator filter results exceed the breathing zone values. Figures 4 ~ 8 show dust/mist sampling results by respirator filter versus breathing zone results for respirator flow rate models #8, #13, #16, #17 and # 18, respectively. Linear regression (with a zero intercept) of all dust/mist sample results produced coefficients of 2.22 (model #8), 1.79 (model #13), 1.57 (model #16), 1.47 (model #17), and 1.89 (model #18) for breathing zone (BZ) versus respirator filter pad (RFP) results (i.e. BZ = coefficient X RFP).

There were several reasons why the respirator filter pad results could be less than the breathing zone values. One possibility was a poor fitting respirator. In this research, one of the assumptions necessary to model airflow through a respirator was no respirator face seal leakage during inhalation. However, after one painting sample there was irrefutable physical evidence of mask leakage. Paint spots were visible around the subject's nose where the respirator should have provided a tight seal. If the respirator

Figure 4: Dust/Mist BZ vs. Resp Results

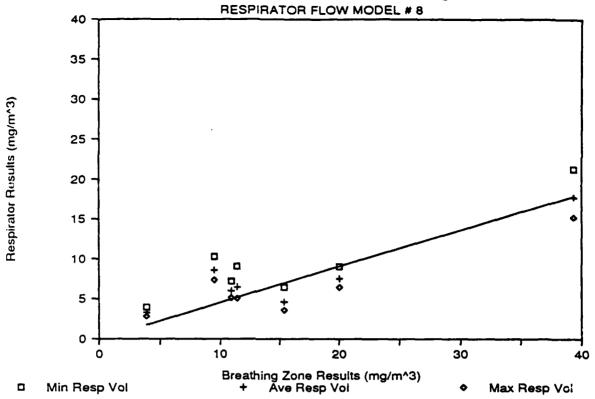


Figure 5: Dust/Mist BZ vs. Resp Results

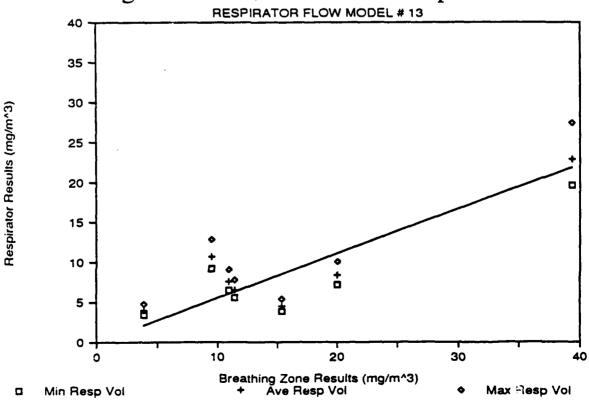


Figure 6: Dust/Mist BZ vs. Resp Results

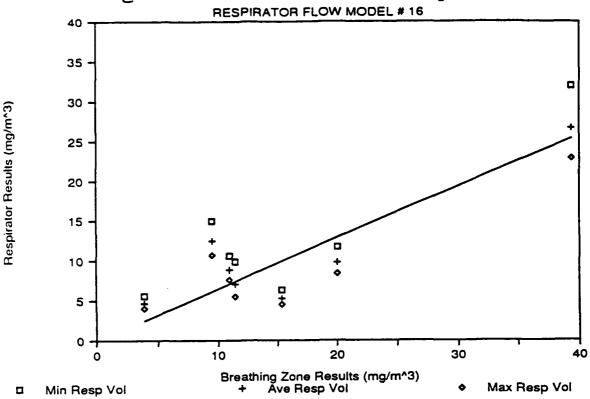


Figure 7: Dust/Mist BZ vs. Resp Results

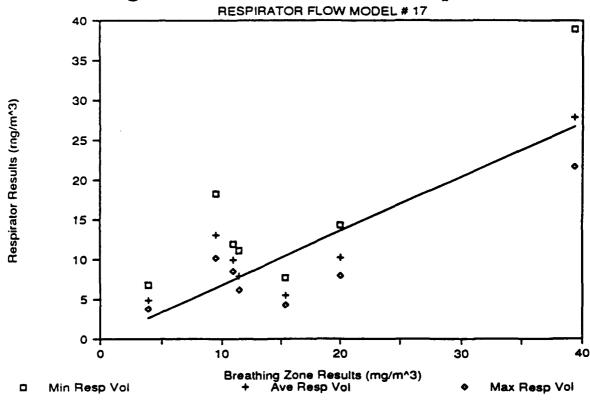


Figure 8: Dust/Mist BZ vs. Resp Results **RESPIRATOR FLOW MODEL # 18** 40 35 30 Respirator Results (mg/m^3) 25 20 15 10 뭏 5 0 10 20 30 40 Breathing Zone Results (mg/m^3) Min Resp Vol Ave Resp Vol Max Resp Vol

fit were deficient, the flow of air through the filter pads would be

diminished, thus decreasing the amount of paint mist deposited on

the filter.

Another possibility was the influence of the faceshield blocking the respirator filters, but not the breathing zone cassette filters, for samples #1, #2, #6, and #7. The faceshield would impede the impaction of large particles onto the respirator pads. This is significant because of the relatively large particle sizes (MMAD 52 um) of the sanding dust. However, the effect of the faceshield would make the respirator pads more representative of the true breathing zone concentration. The cassette filter sample, being outside the faceshield, would overestimate the particulate

concentration susceptible to inhalation. This was analogous to studies that indicated the concentrations of welding fumes outside a welders helmet were 3.3 - 15 times the concentration inside the helmet [16].

A third possiblity for discrepancies were errors in determining the sample weights deposited on the respirator filter pads. The corrections to respirator filter weight due to changes in relative humidity in the laboratory (Table 1) were based on limited data (4 filters @ 14 days). Because comparatively minute variations in relative humidity corresponded in several samples (#2 and #4) to large deductions in sample weight, small errors in the relative humidity correction factor lead to significant differences in the amount of sample detected.

Additional factors that would have effected this difference were loss of sample during storage/transport and errors in analytical balance measurements. However, these additional factors are considered negligible.

Statistical Analysis for Dust/Mist Samples: The breathing zone and respirator cartridge sampling results were compared using a Paired Student-t test protocol (MYSTAT Ver 2.0, Copyright (c) 1988, Systat Inc., Evanston, Il). The analysis determined if there was a significant difference between the sampling means of the respirator filter concentrations versus the breathing zone sampling pump concentrations for the dust/mist sample. All five of the acceptable

respirator airflow models (average flowrates) were employed for the comparison. Because the models provided a range of possible respirator flowrates, the lower limits of this range (mimimum flow rates) were also used to calculate resprator filter concentrations. The minimum flowrate concentrations were then compared to the breathing zone results.

The results of paired student-t tests are listed in Table 8.

Of the five (5) acceptable respirator flow rate models, only model

#17 maintained no significant difference (95% confidence level)

between the breathing zone and respirator filter values for

dust/mist samples. For minimum flow rate values of acceptable

respirator models, all of the models have no significant difference

between the breathing zone and respirator filter pad results. This

outcome suggests that the respirator flow rate models overestimated

the actual worker inspiration rates. However, operational

differences such as the faceshield covering during sanding and leaks

around the edge of the respirator during painting interfered with

quantifying this difference.

Trends of Calculated Data for Organic Vapor Samples:

Respirator airflow model #17 was the only model to show no significant differences between the respirator and breathing zone dust/mist concentrations. Therefore, all of the respirator cartridge sampling results utilized this model for calculating workplace concentrations. The organic vapor sampling results indicated the breathing zone charcoal tube constituents were 1.5 to

Table 8: Paired Student-t Test Results

Average	Breathing Zone I Versus	Mean Difference	Std. Dev. Difference	T Value	P Value
		~ ~ AL	L DUST / MIST	SAMPLES ~	-
Average Flow Rate	Model #8 Model #13 Model #16 Model #17 Model #18	6.650 8.376 5.123 4.449 7.019	6.585 7.384 6.034 5.965 6.770	2.636 3.001 2.246 1.973 2.743	0.030 0.038 0.045 0.088* 0.027
Minimum Flow Rate	Model #8 Model #13 Model #16 Model #17 Model #18	4.723 6.189 2.801 0.227 5.271	5.954 6.834 5.574 5.439 6.121	2.099 2.396 1.330 0.110 2.279	0.081* 0.054* 0.232* 0.916* 0.063*
	~ ~ ALL	DETECTED	ORGANIC VAPOR	CONSTITUENTS	~ ~
Ave Flow Rate**	OV-1 (all) OV-2 (all) OV-3 (all) OV-4 (all) OV-5 (all)	0.571 3.655 2.746 2.613 0.616	2.792 4.004 3.914 4.800 8.141	0.678 3.028 2.219 1.440 0.251	0.513* 0.013 0.054* 0.200* 0.807*
	~ ~ SPECI	FIC ORGANI	C VAPOR CONST	TITUENTS ~ ~	
Ave Flow Rate**	Methylcycl pentane n-Heptane Toluene p-Xylene o-Xylene	0.286 1.396 7.434 0.806 0.348	0.267 1.396 5.421 0.638 0.619	2.397 2.281 3.066 2.826 1.257	0.075* 0.085* 0.037 0.048 0.277*

Note: OV = organic vapor (volatile aromatic hydrocarbons) samples (all constituents; See Table 5)

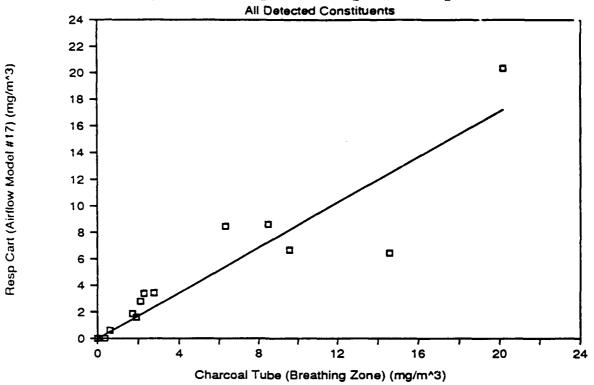
^{* =} No statistically significant difference at 95% confidence level

^{** =} Using Respirator Flow Model # 17

2.5 times greater than the respirator cartridge constituents. was a general trend in the ratios of respirator cartridge to charcoal tube (breathing zone) results within and between samples. Within a sample the ratios were fairly constant among the constituents, allowing for confidence limits due to the analytical procedure. The ratios were about 1.0, 1.75, 2.7, 2.1 and 1.5 for samples OV-1, OV-2, OV-3, OV-4, and OV-5, respectively, with confidence allowances. However, OV-1 and OV-2 involved breathing zone charcoal tube sampling while the worker refilled the paint gun and did not wear the respirator. To correct for this discrepancy, the exposures to the charcoal tube during the refill operations were assumed to be zero and the concentration adjusted by subtracting the duration of the refill operations (38 minutes in OV-1; 20 minutes in OV-2) from the total sampling time. The adjusted ratios of breathing zone charcoal tube concentrations to respirator cartridge concentrations were 1.7 (OV-1) and 3.0 (OV-2). Disregarding the results of OV-1 and OV-2 because of the inconsistencies in exposure measurements, the ratios of charcoal tube to respirator cartridge concentrations were fairly uniform approximately 2.0.

Figures 9 through 13 display the respirator cartridges results versus charcoal tube (breathing zone) results for all the organic vapor constituents detected. From linear regression (with intercept at zero) the coefficient of charcoal tube to respirator cartridge constituents were 1.06 (OV-1), 1.71 (OV-2), 1.94 (OV-3), 1.43 (OV-4), and 0.59 (OV-5). Figures 14 - 18 exhibit comparisons of individual constituent results for methylcyclopentane, n-heptane,

Figure 9: Organic Vapor Sample # 1





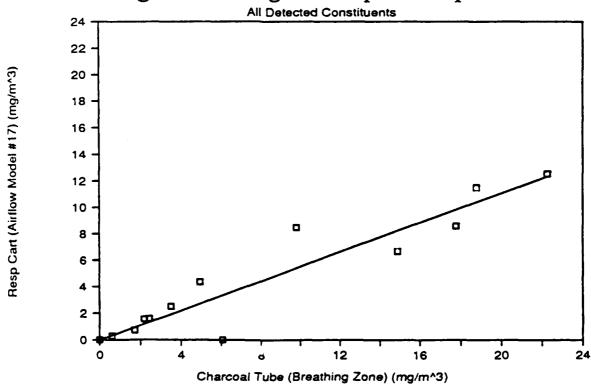


Figure 11: Organic Vapor Sample #3

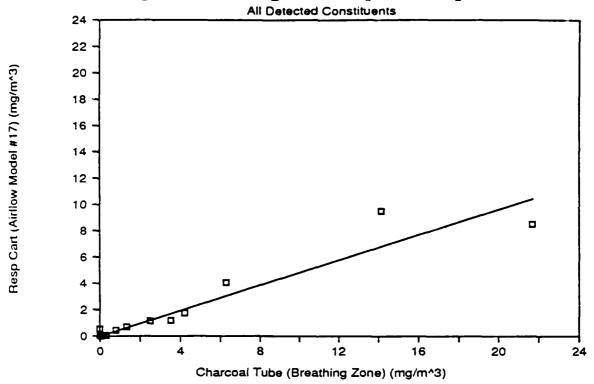


Figure 12: Organic Vapor Sample # 4 All Detected Constituents Resp Cart (Airflow Model #17) (mg/m^3) Charcoal Tube (Breathing Zone) (mg/m^3)

Figure 13: Organic Vapor Sample # 5

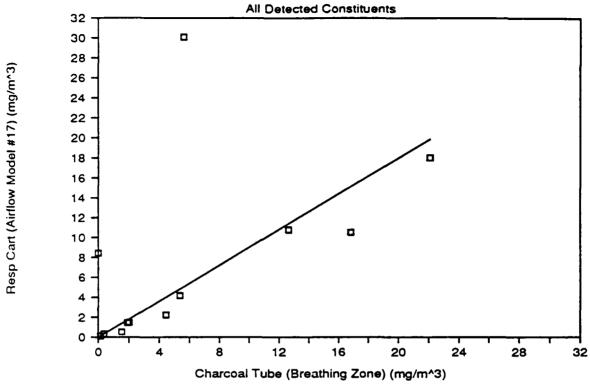


Figure 14: Organic Vapor Sample Results

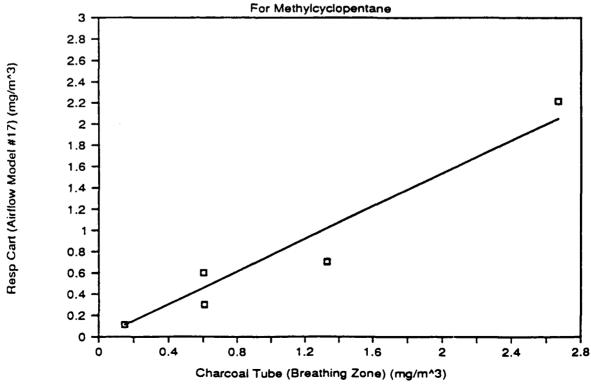


Figure 15: Organic Vapor Sample Results

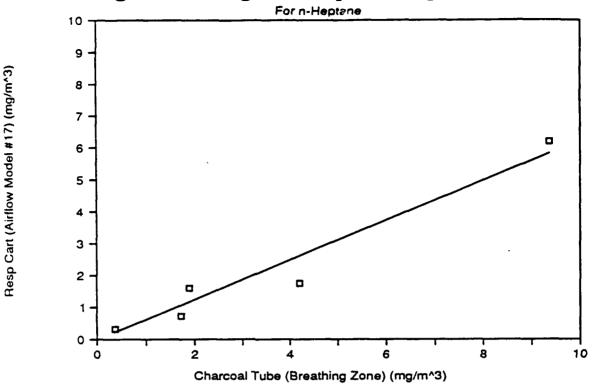


Figure 16: Organic Vapor Sample Results

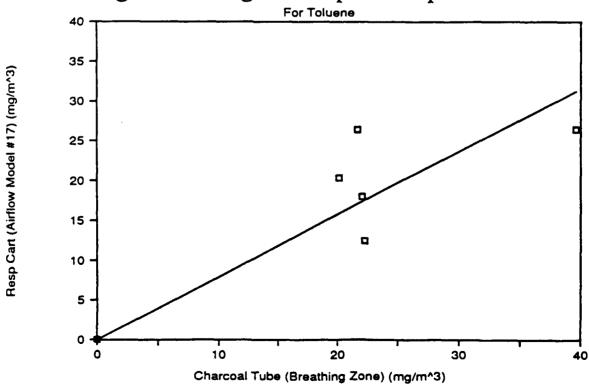


Figure 17: Organic Vapor Sample Results

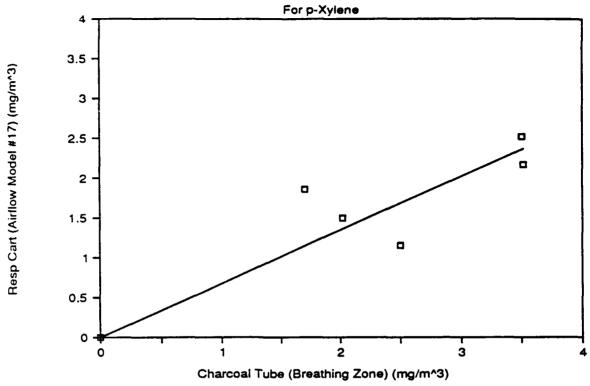
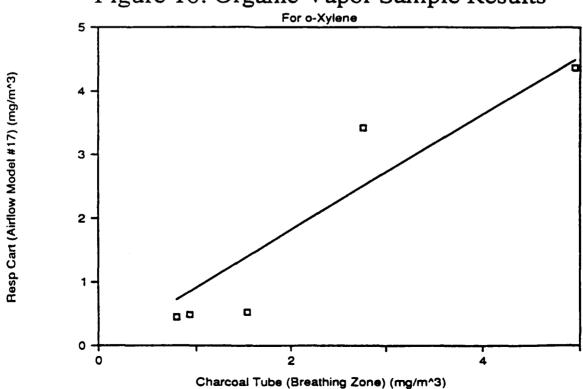


Figure 18: Organic Vapor Sample Results



toluene, p-xylene and o-xylene. Calculated linear regression coefficients for individual constituents were 1.30 (methylcyclopentane), 1.61 (n-heptane), 1.27 (toluene), 1.48 (p-xylene), and 1.10 (o-xylene)

One possible reason why the charcoal tube results were greater than the respirator cartridges was the poor fitting respirators. The affect is identical to the explanation of the discrepancy in dust/mist samples. A consequence of this incident was the implication that the respirator protection factor1 (PF) would actually be reduced to 2.0, instead of the assumed value of PF=10 for half-mask dual cartridge respirators.

Statistical Analysis for Organic Vapor Samples: The organic vapor results were compared statistically by all non-zero constituents in each sample and five (5) individual constituents among samples (Table 8). For four (4) of the five (5) of the volatile aromatic hydrocarbon samples, except OV-2, there was no significant difference (95% confidence level) between the charcoal tube breathing zone results and the respirator cartridges when all of the constituents were compared. For indvidual constituents, three of the five, methylcyclohexane, h-heptane, and o-xylene, demonstrated no significant differences between the charcoal tubes

^{1.} The respirator protection factor is defined as the concentration outside the respirator divided by the concentration inside the resprirator [17]. PF = Conc (out) / Conc (in).

and the respirator filter catridges. These outcomes signified that this method would be viable for workplace exposure screening samples or estimating a resprirator workplace protection factor.

Conclusion:

It has been suggested that industrial airborne workplace concentrations can be calculated based on the amount of contaminant deposited on respirator cartridges and estimating the flowrate through the respirator with ergonomic and respiratory ventilation models.

The physiological models used in this research appear to overestimate the actual flow, although several factors such as respirator mask leakage, sensitivity of resin coated filter pads to relative humidity, and differences in analytical sensitivities between the methods made quantitative conclusions unreliable.

However, the results of the organic vapor respirator cartridges did show countenance for this procedure in screening workplace exposures or estimating a resprirator workplace protection factor [17, 18].

Further studies should be conducted to validate this method.

Additional studies might include more subjects and operations and probably include qualitative fit testing immediatly before and after (and possibly during) the sampling.

Further studies may indicate that, like biological exposure indicies [18], respirator cartridge analysis methods are inconsistant to charcoal tube sampling because too many factors influence the results. However, if the purpose of workplace sampling is to determine the potential employee exposure, then the affect of factors such as faceshields would make the respirator pad analysis more representative of the true breathing zone concentration.

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Appendix I Operation Observations by Sample

Dust/Mist Sample # 1 Subject Info:

Operation: Pneumatic disk sanding Height: 182.88 cm

inside paint booth Weight: 81.64 kg

Age: 25 yrs

Breathing Zone Sampling Info: Sex: M

Time Pump (on/off) 0959/1054 Total Sampling Time: 55 min

Flowrate (on/off; lpm) 2.04/1.97 Total Volume Sampled (liters) = 111

Membrane Filter Wt (post/pre or matched): 0.04992/0.04887

Respirator Sampling Info:

Left Filter Weights (Post/Pre): 2.66993/2.64878 Right Filter Weights (Post/Pre): 2.41849/2.40034

note: 2.0 hrs @ room temp; No post incubation before weighting

Blank correction is + 0.00639 grams/filter

Open face filter cartridges (no filter covers).

Observation:

Elapsed Time hr:min	Position of subject	Position Time (min)	Respirator 'on/off)
0:00 - 0:02	standing (prep)	2) on
0:02 - 0:35	standing	33	on
0:35 - 0:43	kneeling	8	on
0:43 - 0:45	sitting	2	on
0:45 - 0:48	standing	3	on
0:48 - 0:51	kneeling	3	i on
0:51 - 0:55	standing	4	on

Ergonomic note: Total Respirator Time On = 55 min

Operation required Time Resp on Kneeling = 11 min two arm movement. Time Resp on Standing = 42 min

Time Resp on Sitting = 2 min

Dust/Mist Sample # 2 Subject Info:

Operation: Pneumatic disk sanding Height: 182.88 cm

inside paint booth Weight: 81.64 kg

Age: 25 yrs

Breathing Zone Sampling Info: Sex: M

Time Pump (on/off) 1207/1306 Total Sampling Time: 59 min

Flowrate (on/off; lpm) 2.05/2.05Total Volume Sampled (liters) = 121

Membrane Filter Wt (post/pre or matched): 0.04937/0.04890

Respirator Sampling Info:

Left Filter Weights (Post/Pre): 2.69486/2.68157 Right Filter Weights (Post/Pre): 2.48315/2.47215

note: 2.0 hrs @ room temp; No post incubation before weighting

Blank correction is + 0.00683 grams/filter

Open face filter cartridges (no filter covers).

Observation:

Elapsed Time

Ergonomic note: Total Respirator Time On = 59 min

Operation required Time Resp on Kneeling = 2 min two arm movement. Time Resp on Standing = 57 min

Dust/Mist Sample # 3

Subject Info:

Operation: Spray Painting Height: 180.34 cm

Weight: 88.45 kg Age: 26 yrs

Breathing Zone Sampling Info: Age: 26
Sex: M

Time Pump (on/off) 0840/0928
Total Sampling Time: 48 min

Flowrate (on/off; lpm) 2.04/2.04 Total Volume Sampled (liters) = 98

Membrane Filter Wt (post/pre or matched): 0.04912/0.04800

Respirator Sampling Info:

Left Filter Weights (Post/Pre): 2.54415/2.53828 Right Filter Weights (Post/Pre): 2.29953/2.29618

note: 1.5 hrs @ room temp; No post incubation before weighting

Blank correction is -0.002775 grams/filter

Observation:

Elapsed Time	Position of subject	Position Time (min)	Respirator (on/off)
0:00 - 0:07	stooping	7	on
0:07 - 0:24	standing	17	on
0:24 - 0:29	stand(refill)	5	on
0:29 - 0:35	standing	6	on
0:35 - 0:38	stand(fix gun)	j 3	on
0:38 - 0:48	standing	10	on

Total Respirator Time On = 48 min

Time Resp On Standing = 41 min Time Resp On Stooping = 7 min

Dust/Mist Sample # 4 Subject Info:

Operation: Spray Painting Height: 187.96 cm

Weight: 104.33 kg

Breathing Zone Sampling Info: Age: 21 yrs

Sex: M

Time Pump (on/off) 0909/0929 Total Sampling Time: 20 min

Flowrate (on/off; lpm) 2.05/2.05 Total Volume Sampled (liters) = 41

Membrane Filter Wt (post/pre or matched): 0.04869/0.04805

Respirator Sampling Info:

Left Filter Weights (Post/Pre): 2.46325/2.45490 Right Filter Weights (Post/Pre): 2.67680/2.66742

note: 1.5 hrs @ room temp; No post incubation before weighting Weight Correction is 1.001934 * Pre Weight

Observation:

Elapsed Time	Position of subject		Position Time (min)	Respirator (on/off)
0:00 - 0:08	standing	1	8	on
0:08 - 0:10	<pre> stand(refill)</pre>	ı	2	on
0:10 - 0:20	standing	ĺ	10	on

Total Respirator Time On = 20 min

Time Resp On Standing = 20 min

Sample # 5:

Dust/Mist Sample # 5

Subject Info:

Operation: Sanding Fiberglass Height: 182.88 cm

Weight: 134.26 kg

Breathing Zone Sampling Info: Age: 50 yrs

Sex: M

Time Pump (on/off) 0817/0851
Total Sampling Time: 34 min

Flowrate (on/off;lpm) 2.05/2.05 Total Volume Sampled (liters) = 70

Membrane Filter Wt (post/pre or matched): 0.04870/0.04796

Respirator Sampling Info:

Left Filter Weights (Post/Pre): 2.66937/2.66424 Right Filter Weights (Post/Pre): 2.38855/2.37890

note: 1.5 hrs @ room temp; No post incubation before weighting

Weight correction is 1.000705 * Pre Wt

Observation:

Elapsed Time	1	Position of subject		Position Time (min)	Respirator (on/off)
0:00 - 0:22	1	standing	,	22) on
0:22 - 0:30	ĺ	stitting	Ì	8	on
0:30 - 0:34	j	standing	j	4	on

Total Respirator Time On = 34 min

Time Resp On Standing = 26 min Time Resp On Sitting = 8 min

Dust/Mist Sample # 6 Subject Info:

Height: 182.88 cm Operation: Sanding Painted Metal

> with Pneumatic Orbital Sander Weight: 81.64 kg

Age: 25 yrs

Breathing Zone Sampling Info: Sex: M

Time Pump (on/off) 1020/1039+1210/1351

Total Sampling Time: 120 min Flowrate (on/off;lpm) 2.2/2.2

Total Volume Sampled (liters) = 264

Membrane Filter Wt (post/pre or matched): 0.05325/0.04796

Respirator Sampling Info:

Left Filter Weights (Post/Pre): 2.50365/2.47601 Right Filter Weights (Post/Pre): 2.47465/2.45352

note: 1.5 hrs @ room temp; No post incubation before weighting

Weight Correction is 1.000705 * Pre Wt

Observation:

Elapsed Time	Position	Position	Respirator
	ı of subject	Time (min)	(on/off)
0:00 - 0:19	sitting	19	on
0:19 - 0:28	standing	j 9	on
0:28 - 0:35	stooping	j 7	on
0:35 - 0:42	standing	7	on
0:42 - 0:44	stooping	j 2	on
0:44 - 0:60	sitting	16	on
0:60 - 1:15	stooping	13	on
1:15 - 1:17	sitting	j 2	on
1:17 - 1:41	standing	26	on
1:41 - 1:45	kneeling	į 5	on
1:45 - 1:49	stooping	4	on
1:49 - 1:51	kneeling	j 2	on
1:51 - 2:00	standing	j 8	i on

Total Respirator Time On = 120 min

Time Resp On Standing = 50 min Time Resp On Sitting = 18 min Time Resp On Kneeling = 7 min Time Resp on Stooping = 26 min

Dust/Mist Sample # 7 Subject Info:

Height: 182.88 cm Operation: Sanding Pneumatic Orbital

Weight: 81.64 kg

Sex:

Breathing Zone Sampling Info: Age: 25 yrs

Time Pump (on/off) 1408/1457 Total Sampling Time: 49 min

Flowrate (on/off; lpm) 2.2/2.2

Total Volume Sampled (liters) = 108

Membrane Filter Wt (post/pre or matched): 0.05222/0.04798

Respirator Sampling Info:

Left Filter Weights (Post/Pre): 2.59421/2.56724 Right Filter Weights (Post/Pre): 2.66179/2.63469

note: 1.5 hrs @ room temp; No post incubation before weighting

Weight Correction is 1.000705 * Pre Wt

Observation:

Elapsed Time	Position of subject	Position Time (min)	Respirator (on/off)
0:00 - 0:04	sitting	1 4	l on
0:04 - 0:24	kneeling	20	on
0:24 - 0:25	standing	1	on
0:25 - 0:27	sitting	2	on
0:27 - 0:49	standing	22	on

Total Respirator Time On = 49 min

Time Resp On Standing = 23 min Time Resp On Sitting = 6 min Time ResP On Kneeling = 20 min

Note: Two persons were sanding during this sampling.

Organic Vapor Sample # 1

Subject Information:

inside waterfall paint booth Weight: 77.11 kg

Age: 22 yrs

Breathing Zone Sampling Info: Sex: M

Time Pump (on/off) 1242/1510 Total Sampling Time: 158 min

Flowrate (on/off; lpm) 1.05/0.97

Total Volume Sampled (liters) = 159.58

Observation:

Elapsed Time	Position	Position	Respirator
	of subject	Time (min)	(on/off)
0:00 - 0:14	stooping	14	on
0:14 - 0:19	refill spray gun	5	off
0:19 - 0:22	stooping	3	on
0:22 - 0:25	standing	3	on
0:25 - 0:31	stooping	6	on
0:31 - 0:43	refill spray gun	12	off
0:43 - 0:46	standing	3	on
0:46 - 0:56	stooping	10	on
0:56 - 0:59	refill spray gun	3	off
0:59 - 1:04	stooping	5	on
1:04 - 1:10	standing	6	on
1:10 - 1:19	refill spray gun	9	off
1:19 - 1:31	standing	12	on
1:31 - 1:34	refill spray gun	3	off
1:34 - 1:46	standing	12	on
1:46 - 1:50	refill spray gun	4	off
1:50 - 1:59	standing	9	on
1:59 - 2:01	refill spray gun	2	off
2:01 - 2:12	standing	11	on

Ergonomic note:

Total Respirator Time On = 94 min

Operation required one arm movement.

Time Resp on Standing = 56 min Time Resp on Stooping = 38 min

Organic Vapor Sample # 2

Subject Information:

Operation: Spray painting tanker truck

pray painting tanker truck Height: 180.34 cm inside waterfall paint booth Weight: 63.45 kg

Age: 22 yrs

Breathing Zone Sampling Info: Sex: M

Time Pump (on/off) 0827/1004 Total Sampling Time: 97 min

Flowrate (on/off; lpm) 1.05/1.00

Total Volume Sampled (liters) = 99.425

Observation:

Elapsed Time	Position	Position	Respirator
	of subject	Time (min)	(on/off)
0:00 - 0:04	standing	4	on
0:04 - 0:06	stooping	2	on
0:06 - 0:16	standing	10	on
0:16 - 0:23	refill spray gun	7	off
0:23 - 0:33	standing	10	on
0:33 - 0:37	refill spray gun	4	off
0:37 - 0:46	standing	9	on
0:46 - 0:49	refill spray gun	3	off
0:49 - 0:50	stooping	1	on
0:50 - 0:59	standing	9	on
0:59 - 1:02	refill spray gun	3	off
1:02 - 1:13	standing	11	on

Ergonomic note: Total Respirator Time On = 56 min

Operation required one arm movement. Time Resp on Standing = 53 min Time Resp on Stooping = 3 min

Organic Vapor Sample # 3

Subject Information:

Height: 180.34 cm Operation: Spray Painting

Weight: 88.45 kg

Age: 26 yrs Breathing Zone Sampling Info: Sex: M

Time Pump (on/off) 0840/0928 Total Sampling Time: 48 min Flowrate (on/off; lpm) 1.05/0.92

Total Volume Sampled (liters) = 47.28

Observation:

Elapsed Time	1	Position of subject	1	Position Time (min)	Respirator
0:00 - 0:07	1	stooping	i	7	on
0:07 - 0:24	i	standing	İ	17	on
0:24 - 0:29	i	stand(refill)	i	5	on
0:29 - 0:35	i	standing	i	6	on
0:35 - 0:38	į	stand(fix gun)	i	3	on
0:38 - 0:48	i	standing	İ	10	on

Total Respirator Time On = 48 min

Time Resp On Standing = 41 min Time Resp On Stooping = 7 min

Organic Vapor Sample # 4

Subject Information:

Operation: Spray Painting Gray Primer He

in Paint Booth

Height: 187.96 cm Weight: 104.33 kg

Age: 21 yrs

Breathing Zone Sampling Info:

Sex: M

Time Pump (on/off) 0909/0929 Total Sampling Time: 20 min

Flowrate (on/off; lpm) 1.05/1.05 Total Volume Sampled (liters) = 21

Observation:

Elapsed Time	Position	Position	Respirator
-	of subject	Time (min)	(on/off)
0:00 - 0:08	standing	8	on
0:08 - 0:10	stand(refill)	2	on
0:10 - 0:20	standing	10	on

Total Respirator Time On = 20 min Time Resp On Standing = 20 min

Organic Vapor Sample # 5 Subject Information:

Operation: Spray Painting Gray Primer Height: 187.96 cm

in Paint Booth Weight: 104.33 kg
Age: 21 yrs

Breathing Zone Sampling Info: Age: 21
Sex: M

Time Pump (on/off) 0910/1001
Total Sampling Time: 51 min

Flowrate (on/off; lpm) 1.04/1.04

Total Volume Sampled (liters) = 53.04

Observation:

Elapsed Time	Position	Position	Respirator
	of subject	Time (min)	(on/off)
0:00 - 0:20	standing	20	on
0:20 - 0:22	stand(refill)	2	on
0:22 - 0:36	standing	15	on
0:36 - 0:38	stand(refill)	2	on
0:38 - 0:51	standing	13	on

Total Respirator Time On = 51 minTime Resp On Standing = 51 min

Appendix II

Dust/Mist and Organic Vapor Sampling Results by Weight

Appendix II: Dust/mist Sampling Results by Weight

~	Sand	39.33	182.88 25.00 49.00	0.05222 0.04799 4.24 2.20 0.108	63 2.59421 2.56724 -1.78 25.19	2.66179 2.63469 -1.83 25.27	50.46	11.9
9	Sand	20.04	182.88 25.00 120.00	0.05325 0.04796 5.29 2.20 0.264	63 2.50365 2.47601 -1.72 25.92	2.47465 2.45352 -1.70 19.43	45.34	8.6
S	Sand	10.94	M 182.88 50 33	0.04870 0.04796 0.74 2.05 0.068	63 2.66937 2.66424 -1.85 3.28	2.38855 2.37890 -1.65 8.00	11.28	15.2
4	Paint	15.37	M 187.96 21 20	0.04867 0.04804 0.63 2.05 0.041	65 2.46325 2.45490 -4.27 4.08	2.67680 2.67470 -4.66 -2.56 *	4.08	6.5
m	Paint	11.44	M 180.34 26 48	0.04912 0.04800 1.12 2.04 0.098	2.54415 2.53828 2.42 8.29	2.29953 2.29618 2.42 5.77	14.07	12.6
7	Sand	3.89	M 182.88 25 59	0.04937 0.04890 0.47 2.05	2.69486 2.68157 -6.83 6.46	2.48315 2.47215 -6.83 4.17	10.63	22.6
, ,	Sand	9.50	M 182.88 25 55	0.04992 0.04887 1.05 2.01 0.111	2.66993 2.64878 -6.39	2.41849 2.40034 -6.39 11.76	26.52	25.3
Sample #	Operation	BZ Result mg/m^3	Sex Height cm Age years Time of Work min	BZ Semple Wt final BZ Semple Wt begin BZ Semple wt mg BZ flow lpm BZ Semple Vol m^3	RH% at Post Wt Left Cart Wt final Left Cart Wt Begin Resp Filter Corr mg Left Resp Samp Wt mg	Right Cart Wt final Kight Cart Wt begin Resp Filter Corr mg Right Resp Samp Wt mg	Total Resp Wt mg	iotal Resp Wt / BZ Wt

* Note: This value taken as 0.00 for Total Respirator Sample Weight

Apardix II: Organic Vapor Sampling Results by Weight

	BZ Samp 0V-1 5.0	34-1 5.0.	Resp Cart OV-1 S.D.	t 0V-1 5.0.	82 Samp 04-2 5.0	04-2 5.0.	Resp Cart OV-2	t 0V-2 5.0.	BZ Samp 0V-3 5.0	. 3.0.	Resp Cart UV-3 5.0.	t 0V-3 5.0.
	\$	T	6	E	ģ	<u>-</u>	Đ	ŗ.	2	ğ	E	ā,
Isopentane	8	. 8	•	9	5	٤	9	ò	ć	8	-	7
nechylogiciopencane	C. C.	3	7.7	0.13	9.0	3 :	3	9.5	S :	3 7	7.1	17.0
n-Heptane	æ :	0.01	3.30 9.30	0.45	0.17	8	1.72	0.14	0.20	3	4.04	0.64
Methylcyclohexane	0.34	0.05	6.3	0.61	0.22	8.	3.80 88.	0.56	0.30	0.01	9.35	7.08
n-Octane	0.31	0.05	5.76	0.52	0.24	8.	3.30	0.22				
1,1,1-Trichloroethane	0.05	8.									1.28	0.33
Methyl Ethyl Ketone	2.18	0.04	13.31	5.52	1.87	90.0	22.92	4.22			0.12	0.14
[sopropanol					0.60	0.14			0.17	0.01	2.73	0.42
Trichloroethylene	1.27	0.05	17.78	۲.3 د	1.73	0.04	20.93	1.52	0.67	0.01	22.01	4.15
Toluene	3.01	0.23	42.15	4.82	2.21	90.0	89. 88	2.19	1.02	0.03	19.69	3.15
Ethlyene Dichloride	1.43	0.04	13.79	1.40	 &	0.03	16.23	0.39	0.01	0.01	0.0	0.2
aua [hx-d	0.25	8.	3.85	0.43	0.35	0.02	6.15	0.55	0.12	8.	5.66	0.34
a-Xylene	0.35	0.02	17.49	1.94	0.38	0.07	20.67	2.23				
o-Kylene	0.4	0.05	7.08	0.78	0.49	8.	10.67	3.16	0.04	8.	1.03	0.14
	82 Sample 0V-4	9 04 0 44	Resp Cart OV-4	t 08-4	82 Sample OV-5	e 00-5	Resp Cart OV-5	t 0V-5				
	<u>.</u>	Ē	T	E	Ē.	Ē	<u>G</u>	Ē.				
Isopentane	0.05	8										
Methylayclopentane	0.0	8		0.93	0.01	8.	0.21	0.06				
n-Heptane	0.31	8.	5.26	0.87	0.02	8.	0.60	0.16				
Methylcyclohexane	0.33	8.	8.7	0.38								
n-Octane	0. 8	8.			0.67	8.	23.25	3.09				
1,1,1-Trichloroethane							15.90	17.25				
Methyl Ethyl Ketone					0.10	8.	2.74	0.40				
Isopropanol	0.08	0.01			0.30	0.4	56.74	13.13				
Trichlaroethylene					0.89	0.01	19.83	2.74				
Toluene	1.33	0.02	22.49 1.17	1.17	1.17	0.01	33.36	4.06				
Ethlyene Dichloride					0.24	0.01	4.19	0.63				
p-Kylene	0.12	8.	<u>.</u> æ	1.26	0.11	8.	2.85	0.34				
e-Kylene	1	ı			0.28	0.01	7.87	9.%				
o-Xylene	0.B	8.	0.4	5.09	0.08	8.	8 .0	0.25				

Appendix III

Dust/Mist Sampling Concentrations
by Respirator Flow Model

Code: 1/11-E8-R11 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 1:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref II: 0.01394 lpm 02/watt Ergonomic Estimate of Total Energy Required from Reference 8: 3400 cal/min (238 Watts) Basal Metabolic Rate estimated from Reference 11: 71.74 watts/ lpm of oxygen required

Sanding 182.88 83.78 25.00 3.47 1.94 0.63 3400.00 237.09 71.94 45.57 191.52 2.67 3.30 1.70 0.95 26.50 4.40 4290.90 5003.35	14.10 11.76 10.08
6 Sanding 182.88 83.78 25.00 3.47 1.94 45.57 09 71.94 45.57 1.94 45.57 1.96 1.70 0.95 26.50 4.40 12253.11 8763.55	5.17 4.32 3.70
Sanding 182.88 83.78 50.00 2.69 71.94 45.57 191.52 3.30 6.90 33.00 4111.14 4863.57	3.36 2.74 2.32
Painting 187.96 87.79 21.00 3.77 2.11 0.66 3400.00 237.09 71.94 47.27 189.82 2.65 3.30 1.57 0.88 26.50 4.40 20.00 1751.35 20.00	2.79 2.33 2.00
Bainting 180.34 81.77 26.00 3.36 1.88 0.62 3400.00 237.09 71.94 44.72 192.37 192.37 2.68 3.30 1.76 0.98 26.50 4.40 48.00 4203.38 4901.30	4.01 3.35 2.87
Sanding 182.88 83.78 25.00 3.47 1.94 45.57 191.52 2.67 3.30 1.70 0.95 2.67 3.30 1.70 1.70 6024.45 4308.75	2.47 2.06 1.76
Sanding 182.88 83.78 25.00 3.47 1.94 0.63 3400.00 237.09 71.74 45.44 191.65 2.67 3.31 1.70 0.95 26.50 4.40 56.50 4.40 56.50 4.40	6.60 5.50 4.72
Units cm kg years lpm lpm lpm cal/min Watts watt/lpm Watts uatt/lpm lpm lpm lpm k/- min liters	E/#/6# B/#/6# B/#/6#
Sample # Operation Height Weight Age Uol Rate O2 (AT) Uol Rate O2 (AT) Total Energy Req Total Energy Req Std Metabolism Basal Rate Energy Req (Work) Vol Rate O2 (Work) Total Rate O2 (Work) Total Rate O2 (Work) Total Rate Expir/Vol Rate Uol Expir/Vol O2 Time of Work Total Uol Exp (Ave) Total Uol Exp (Max) Total Uol Exp (Min)	Conc (min) Conc (ave) Conc (max)

Code: U11-E8-R6 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 2:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 11: 0.01394 lpm O2/watt

(238 Watts) required	~	Sanding	182.88	83.78	25.00	3.47	1.94	0.63	3400.00	37.	107.53	68.11	168.98	2.36	2.99	1.54	0.86	26.50	4,40	49.00	3882.70	4527,38	3238,03	15.58	12.99	11.14
l∕min oxygen	9	Sanding	182.88	83.78	25.00	3.47	1.94	0.63	8	37.	107.53	68.11	168.98	2.36	•	1.54	•	26.50	4.40	120.00	9508.66	11087.45	7929.86	5.72	4.77	4.09
3400 ca s/ lpm of	រប	Sanding	182.88	83.78	50.00	5.69	1.51	φ.	3400.00	~	•	€8.11	168.98	2.36	2.99	1.98	1.11	37.70	6.90	33.00	3720.04	4400.89	3039.18	•	3.03	•
Reference 8: 107.53 watt	4	Painting	187,96	87.79	21.00		2.11	•				70.65	166.44	•	2.98	1.41		26.50	4.40	20.00	1578.52	1840.61	1316.42	3.10	2.58	
₽0 6:	С	Painting	180.34	81.77	26.00	3,36	1.88	0.62	3400.00	•	ζ.	66.84	•	2,37	•	1.59	0.89	26.50	4.40	48.00	3810.97	4443.74	3178.21	4.43	3.69	۲.
Required f n Reference	2		182.88	83.78	25.00	3.47	1.94	0.63	3400.00	37.	•	68.11	168.98	2.36	2.99	1.54	•	26.50	4.40	59.00	4675.09	5451.33	3858.85	۲.	2.27	თ.
al Energy mated from	Ħ	Sanding	_	83.78	25.00	G. 47	1.94	0.63	3400.00	237.09	107.53	68.11	168.98	2.36	•	•	0.86	26.50	4.40	55.00	4358.13	5081,75	3634.52	7.30	60.9	5.22
ite of Tot Rate esti		Units	E C	kg	years	l pm	l par		cal/min	Watts	watt/1pm	Watts	Watts	md ?	lpm	×	×	ite 02	-/+	e Lie	liters			mg/m/3	mg/m/3	mg/m/3
Ergonomic Estimate of Tot Basal Metabolic Rate esti	Sample #	Operation	Height	Weight	Age	Vol Rate 02 (max)	Vol Rate 02 (AI)	Vol Rate 02 (0 Watts)	Total Energy Req	Total Energy Req	Std Metabolism	Basal Rate	Energy Req (work)	Vol Rate O2 (Work)	Total Rate O2 Req	% of AT Required	% of Vol 02 (max)	Vol Rate Expir/Vol Rate	Vol Expir/Vol 02	Time of Work	Total Vol Exp (Ave)	Total Vol Exp (Max)	fotal Vol Exp (Min)	Conc (min)	Conc (ave)	Conc (max)

Code: U11-E8-R12 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 3:

0.01394 lpm G2/watt Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 11:

Ergonomic Estimate of Total Er Basal Metabolic Rate estimated		al Energy R mated from	Required Referenc	from e 12:	Reference 3: See lable 5	3400	cal/min (238	38 Watts)
Sample #		ન	2	C	4	ហ	9	۷
Operation	Units	Sanding	Sanding	Painting	Painting	Sanding	Sanding	Sanding
Height	E C	182.88	$182.8\overline{8}$	ö	2.9		182.88	182.88
Weight	א	83.78	83,78	81.77	87.79	83.78	•	83.78
Age	years	25.00	25.00	26.00	7	0	25,00	25.00
Vol Rate 02 (max)	Ipm	3.47	3,47	3,36	3.77	2.69	3.47	3.47
Vol Rate 02 (AI)	l p.m	1.94	1,94	1.88	2.11	1.51	1.94	1.94
Vol Rate 02 (0 Watts)	lpm (0.63	0.63	0.62	0.66	φ.	0.63	0.63
Total Energy Req	cal/min	0	0	3400.00	3400.00	90	•	3400.00
	Watts	237.09	237.09		237.09	237.09	237.09	237.09
Std Metabolism	cal/m^2/hr	40.24	40.24	40.24	40.24	40.24	40.24	40.24
Basal Rate	Watts	0.10	0.10	0.09	0.10	۲.	0.10	0.10
Energy Red (work)	Watts	237.00	•		236.99	•	237.00	237.00
Vol Rate O2 (Work)	lpm	3.31	3.31	3,31	3.31	3.31	3,31	3.31
Total Rate O2 Req	l mg l	σ.	3,94		•	σ.	3,94	3.94
% of AT Required	×	0			•	2.61	•	
% of Vol O2 (max)	×	1.13	1,13		1.05	1.46	1.13	1.13
Vol Rate Expir/Vol Rate	ate 02	37.70	37.70		37.70	37.70	37,70	37.70
Vol Expir/Vol 02	-/+	6.90	6.90	6.90	6.90	6.90	6.90	6.90
Time of Work	ni e	55.00	59,00	48.00	20.00	33.00	120.00	49.00
Jotal Vol Exp (Ave)	liters	ω	8760.90	7106.17	2987.58	4900.16	17818.78	7276.00
. Vol		1.6	10364.35	8406.77	3534.38	5797.01	21080.04	8607.68
Totai Vol Exp (Min)		6672.20	7157,45	5805.57	2440.78	4003.32	14557,52	5944.32
Conc (min)	mg/m/3	Ø.	1.48	2.42	1.67	2.85	3.11	8.49
Conc (ave)	E~m/6m	3.25	1.21	1.98	1.36	2.30	2.54	6.93
Conc (max)	mg/m/3	۲.	1.03	1.67	1.15		2.15	•

Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 4: Code: VII-E10-R11

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 11: 0.01394 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 10: See Table 4. Basal Metabolic Rate estimated from Peference 11: 71.4 watts/ lpm of oxygen required

# a U000		-	2	m	4	ហ	9	
_		ngin	rdın	nting	ntin	ndin	ndin	ndin
Heropt	6	182.8	182.8	180.3	187.9	œ	œ	œ.
	<u>د</u> ا	(C)	83.7	81.7	87.7	3.7	3.7	83.7
	0 C	. 0	5.0	6.0	1.0	0.0	5.0	5.0
		(i) (i)	(m)	i m	3.77	N	3.47	3.47
	1 6	· თ	· თ	ω	+-1	v.	9	σ.
Upl D2 (0 Watts)	ind I	0.63	0.63	0.62	9.	9.	9.	Θ.
	•							
factor Rea Standing	cal/min	0.0	50.0	50.0	50.0	0.0	0.0	ö
Francis Red Standing	Watts	198.7	198.7	2.9	δ.	98.7	98.7	98.
Std Motabolism	watt/lpm	71.7	71.7	1.7	1.7	1.7	1.7	Ţ.
Bacal Rate	Watts	5.4	5.4	4.5	7.1	5.4	S. 4	w.
French Rea (work)	Watts	153.32	153.32	98.38	95.84	153.32	153.32	ന
UOI OO (MORK)	l Diff	2.1	2.1	1.3	ω.	٠,	٦.	•
Total O2 Required	. ea	٧.	۲.	σ.	σ.	۲.	۲.	•
2 of AT Required	۰.	4	4	0.	φ.	œί	4	•
3	*	œ	Φ.	ני	S.	٥.	œ	•
		N.	ĸ.	26.50	28.50	۲.	ហ	•
Expir/Vol	-/+	4.	4	4.	٣.	6.9	4.	4.
.,-	min	42.00	0.	41.00	٥.	o.	50.00	23.00
Tanna Ban Sitting		50.0	50.0	50.0	50.0	50.0	50.0	50.0
Franci Red Sitting	Watts	17	177.	122.03	122.03	177.82	177.82	177.82
Std Metabolism	watt/lom	07.5	02.5	07.5	07.5	07.5	07.5	07.5
Basal Rate	Watts	8.1	+-1	6.8	9.0	7	8.1	68.1
Energy Reg (work)	Watts	9.7	\sim	5.1	1.3	۲.	9.7	٧.
Vol 02 (Work)	l pm	٠	ហ	۲.	۲.	ហ	ហ	ហ
Total O2 Required	Ed l	₩.	-	m.	ო.	┥.	ન.	┥.
% of AT Required	.×		Η.	۲.	٠.	₹.	┥.	┥.
	×	9.	9	4	ო.	Φ.	9.0	φ, 1
Vol Expir/Vol 02		26.50	26.50	ហ	v.	ហ	ហ	ນໍ
	-/+	4	₹.	ᅻ.	8.10	4	4	4
	C.I.E.	2.00	00.00	٥.	٥.	٥.	18.0	۰. و
						CONTINUED	ON NEXT	PAGE

Dust/Mist Sampling Results for Respirator Flow Model # 4: (con't) Appendix III:

/ Sanding	3050.00 212.69 107.53 68.11 144.57 2.02 2.65 1.36 0.76 26.50 4.40	2750.00 191.77 107.53 68.11 123.65 1.72 2.36 1.21 0.68 26.50	3283.10 3828.22 2737.98 16.44 13.71
6 Sanding	3050.00 212.69 107.53 68.11 144.57 2.02 2.65 1.36 0.76 26.50 4.40	2750.00 191.77 107.53 68.11 123.65 1.72 2.36 1.21 0.68 26.50 4.40	6967.62 8124.51 5810.73 6.92 5.77 4.95
5 Sanding	3050.00 212.69 107.53 68.11 144.57 2.02 2.65 1.76 0.98 26.50 4.40	2750.00 191.77 107.53 68.11 123.65 1.72 2.36 1.56 0.88 26.50 4.40	3175.51 3748.92 2602.11 2.31 1.89
4 Paintíng	2250.00 156.90 107.53 70.65 86.25 1.20 1.86 0.88 0.49 28.50 8.10	1950.00 135.98 107.53 70.65 65.33 0.91 1.57 0.74 0.42 28.50 8.10	1136.41 1459.39 813.43 5.01 3.59 2.79
3 Painting (2250.00 156.90 107.53 66.84 90.06 1.26 1.88 1.00 28.50 8.10 7.00	1950.00 135.98 107.53 66.84 69.14 0.96 1.59 0.84 0.47 28.50 8.10	2540.75 3006.87 2074.62 6.78 5.54 4.68
2 Sanding ا	3050.00 212.69 107.53 68.11 144.57 2.02 2.65 1.36 0.76 26.50 4.40	2750.00 191.77 107.53 68.11 123.65 1.72 2.36 1.21 0.68 26.50 4.40	4311.68 5027.58 3595.78 2.95 2.46
1 Sanding	3050.00 212.69 107.53 68.11 144.57 2.02 2.65 1.36 0.76 26.50 4.40	2750.00 191.77 107.53 68.11 123.65 1.72 2.36 1.21 0.68 26.50 4.40	3886.96 4532.34 3241.58 8.18 6.82 5.85
	cal/min Watts watt/lpm Watts Watts Ipm Ipm 1pm 1pm 1pm	cal/min Watts watt/lpm Watts Ipm lpm % % % % % % % % % % % % % % % % % % %	liters mg/m/3 mg/m/3 mg/m/3
Sample # Operation	Energy Req Stooping Energy Req Stooping Std Metabolism Basal Rate Energy Req (work) Vol O2 (Work) Total O2 Required % of AT Required % of AT Required % of O1 Expir/Vol O2 Vol Expir/Vol O2 Vol Expir/Vol O2	Energy Req Kneeling Std Metabolism Basal Rate Energy Req (work) Vol O2 (Work) Total O2 Required % of AT Required % of AT Required % of Expir/Vol O2 Vol Expir/Vol O2 Vol Expir/Vol O2	Vol Exp (Ave) Vol Exp (Max) Vol Exp (Min) Conc (min) Conc (ave) Conc (max)

Code: U11-E10-R6 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 5:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 11: 0.01394 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 10: See Table 4. Basal Metabolic Rate estimated from Reference 6: 107.53 watts/ lpm of oxygen required

7		i m	'n,	•	•		50.0	8.7	07.	8.1	9.0	œ	4	ď	۲.	26.50	4	23.00	50.0	177.82	1.	•	'n	•	•		•	26.50	4.40	9.00	PAGE
ø	Sanding 182,88	83.7	5.0	₩. ₩.	9	9.	50.0	7	07	₹.	9	æ	4	Ņ	Ŀ	26.50	4.40	50.00	50.	•	-	<u>ن</u>	'n	•	2.48	•		•	4.40	18.00	ON NEXT
ហ	Sanding 182,88	83.	ö	•	•	•	50.0	98.7	107.53	8.1	9.0	œ	4	9.	6.		4	26.00	ທ	177.82	1.7	4	4	æ	2.48	9.	6.	26.50	•	8.00	CONTINUED
4	Painting 187 96	87.7	1.0	۲.	۲.	9.	50.	'n	107.53	ö	'n					28.50	•	20.00	50.0	122.03	1.7	₹.	4.9	0.	۲.	ω.	4	ល	8.10	00.	
m	Painting 180 34	81.7	6.0	ניו	ω	φ,	50.0	2.9	07	6.8	6.1	0.	φ.	œ.	יט	28.50		41.00	50.0	0.	۲.	'n	4	۰.	~	σ,	ທຸ	ທຸ	8.10	0	
N	Sanding 182 88	83.7	5.0	4	σ.	9.	0.0	8.7	107.53	8.1	9.0	œ	4	Š	۲.			0.	50.0	æ	1.7	5.4	7.4	1.85	4	ς.	۲.	ĸ.	4.40	0.00	
1	E c	83.7	5.0	4	σ.	۰.	0.0	98.7	107.53	8.1	9.0	æ	4	Ġ	۲.	26.50	4.40	0.	o.	22.	- i	'n,	•		•	•	•	•	4.40	•	
	Ę	. ₹	qears	l pa	lp.	l pa	cal/min	Watts	watt/lpm	Watts	Watts	lpm	Ipm	×	×		-/+	e Lin	cal/min	Watts	watt/1pm	Watts	Watts	lpm	l pa	×	×		-/+	E.E	
Sample #	Operation	Weight	Age	Vol 02 (max)	Anerobic Threshold	Vol O2 (0 Watts)	Energy Req Standing	Energy Reg Standing	Std Metabolism	Basal Rate	Energy Req (work)	Vol 02 (Work)	Total 02 Required	% of AT Required	% of Vol 02 (max)	Vol Expir/Vol 02		Time of Standing	Energy Reg Sitting		Std Metabolism	Basal Rate	Energy Req (work)	Val 02 (Work)	Total O2 Required	% of AT Required	% of Vol O2 (max)	Vol Expir/Vol 02	ľ	Time of Sitting	

Dust/Mist Sampling Results for Respirator Flow Model # 5: (con't) Appendix III:

	Sanding	50.	'n	-		۲.	2.33	•	•	ö	•	•	0.00	0	91.7	71.7	. 7	֓֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֓֓֓֓֓֜֜֜֜֜֓֓֓֓֓֓	יני	0	Ψ	ייי	, ·		4.40	20.00	000	33000.		28.3	6.3	13.61	1.6	
•	Sanding	50.0	2.6	71.7	4	7.2	2.33	ď	ហ	æ	ĸ.	4	0	50.	+	71	. u	֓֞֝֞֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֝֓֓֓֓֡֓֓֡֝֡֓֡֓֡֓֡֝֓֡֓֡֓֡֡֝	•	•	•	•	•	26.50		•	700	0.0760	134.6	817.7	9.	5.76	Q.	
	Sanding	0.0	5.6	1.7	4	7.2	2.33	φ.	σ.	Η.	۲.	φ.	٥.	50.0	191.7	7.1	 	4.U	6. 9	٥.	ø.	۲.	σ,	26.50	4.	0.00	,	2217.42	385.0	849.2	Ś	2.70	ω,	
	ainting	50.	156.	71.		ď						4.40	0.00	50.0	135 9	, ,	· ·	٦.	щ С	ď	σ.	σ.	ហ	28.50	8.1	٥.	(949 949	19.0	79.4		4.29		•
m	aintin	50.0	156.9	71.7	. RU	, m		٦,	-	ω.	ហ	4.	0.	50.0	125 0	֓֝֝֝֡֝֝֝֝֡֝֝֝֡֝֝֝֡֝֝֡֡֝֝֡֡֝֝֡֝֡֡֝֝֡֝֡֝֡֝֡	\	ທ.	4.1	ú	σ.	0	Ŋ	26.50	4.	0.	1	2372.64	999.0	746.2	0.	5,93	9	•
נט	Sanding P	50.07	712.6	71.7	. 4	, ,		σ	מי	σ	יט	4	٥.			יון יו	1. (4.	6.3	2.0	φ,	יח		· U7	4	2.00		820	489.7	11.0	ď	2.76	ָת	
	Sanding	5 0	010.0	71.0	. 4			•		. Œ	תו נ	4	0.00	_	3	היי	;	ហ		N			•	76.50	. 4	11.00		643.7	248.7	38.	7	2, 2B	! v	,
		S 2/ 10		WG1.5	2011/10/11 11++6		20 C	1 0	<u>.</u>	: >	:	-/+	e Lie	2.67		Watts	watt/lpm	Watts	Watts	ויים		, ,	: >	:	1/+	C I E		liters			EVE/00			c. = /6=
Samp]e #	Operation	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Energy Red Stooping	בות בות	E S	משפח ושפשם	Energy Req (work)	1-4-1 02 Banning	TOTAL UZ KEQUITED		10.1 Expire/10.100	10 CAPILLY 01 01 10 10 10 10 10 10 10 10 10 10 10	Time of Stooping		Energy Red Kneeling	1 ng		Basal Rate	Frond Red (Lork)			S OF DESCRIPTION	to the negative of the contract of the contrac	7 01 02 (max)	VOI EXPIRAÇÃO OZ	Time of Stooping		Vol Exp (Ave)	Uol Exp (Max)	EXT				Conc (max)

Code: U11-E10-R12 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 6:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 11: 0.01394 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 10: See Table 4. Basal Metabolic Rate estimated from Reference 12: See Table 5.

2	Sandin	182.	83.	25.0	ω 4.	1.9	0		86	40	0	198	ς.	'n	; - -i	o.	26.	4.	23.		177.	40.	Ö	17	ς.	'n	Ή.	ö	26.	4.	Ġ	PAGE
v		'n	•	ທ່	3.47			2850.00	98.7	40.	•	198,64	'n	3,40		_•	26.50		50.00	2550.00	177.	0.2	•	177.72	2.46	3.11	1.60	0.90	26.50		18.00	ON NEXT
S.	<u>_</u>	•		o.	2.69		•	2850.00	98.7	Ŋ		198.64	۲.	4	2.26					50.0		40.2	0.10		2.48		0.		۲.	σ.	8.00	CONTINUED
4	t i	87.9	۲.	1.0	3.77	. 1	9.	2050.00	42	40.	•	•			1.26	•	•	4.40	20.00	1750.00	122.0	40.2		121.93	1.70			•		•	0.00	
m	nti	Ö	•	φ.	3.36	•	•	2050.00	42	0	•	•		•	1.39			4.40	41.00	1750.00	122	ö	•	121.94	•	2.32	•	•	26.50	4.40	00.00	
2	Sanding							2850.00	198.74			•			1.75		26.50		57.00	2550.00	177	•	•	177.72	•	•			26.50	4.40	00.00	
Ħ	din	œ	۲.	5.0	3,47	ن .	φ	2850.00	œ.	40.24	0.10	198.64	•	•	1.75	•	26.50	•	42.00	2550.00	ζ.	40.54	•	177.72		•	•	•	26.50	4.40	•	
		EO	kg	year's	Pa Ed!	l pa	l pm	cal/min	Watts	cal/m^2/hr	Watts	Watts	l pa	Ipa	×	×		-/+	nie	cal/min	Watts	cal/m^2/hr	Watts	Watts	I pa	lp.	×	×		-/+	€	
Sample #	Operation	Height	Weight	Age	Vcl 02 (max)	Anerobic Threshold	Vol 02 (O Watts)	Energy Req Standing	Reg	Std Metabolism	Basal Rate	بر 18	Vol 02 (Work)	Total O2 Required	f AT	Vol 02 (ma	Expir/Vol	ХPi	Time of Standing	Energy Req Sitting		Std Metabolism	Basal Rate	ጿ	Vol 02 (Work)		F AT	Vol 02 (mē	Expir/Vol	XPI	Time of Sitting	

(con't) Dust/Mist Sampling Results for Respirator Flow Model # 6: Appendix III:

7 Sanding	3050.00 212.69 40.24 0.10 212.59 2.96 3.60 1.85 1.04		0.000 ± 0.000	10.41 8.93
6 Sanding	3050.00 212.69 40.24 0.10 212.59 2.96 3.60 1.85 1.04	6. 26. 50.	191.7 191.6 191.6 191.6 191.6 134.9 26.5 26.5 27.6 28.7 29.2 29.2	3.38 3.38
5 Sanding	3050.00 212.69 40.24 0.10 212.59 2.96 3.60 2.39 1.34	6.9 0.0 50.0	191.04 191.05 191.06 10.01 10.	1.40
4 Painting		4.4 0.0 50.0	135. 135. 135. 26. 26. 26. 171.	2.90 2.90 4.90
3 Painting	2250.00 156.90 40.24 0.09 156.80 2.19 2.19 2.81 1.49 0.84	. 4. 7. 50.	26.19 20.02 20.02 20.03 20	4.18 3.59
2 Sanding	3050.00 212.69 40.24 0.10 212.59 2.96 3.60 1.85 1.04	6. 50.	191. 191. 191. 26. 26. 27. 28. 29.	2.00
1 Sanding	3050.00 212.69 40.24 0.10 212.59 2.96 3.60 1.85 1.04	6.9 0.0 50.0	191.7 191.6 191.6 191.6 1.0 26.5 26.5 11.0 11.0 100.8	4.63 4.63
	cal/min Watts cal/m^2/hr Watts Upm Ipm Ipm	#/- min cal/min	Watts Watts Watts Ipm Ipm Ipm Inm Iiters	6/E/6E
Sample # Operation	y Req Stoop y Req Stoop d Metabolis Basal Rate gy Req (wor 1 02 (work) 1 02 Requir f AT Requir Vol 02 (ma	Vol Expir/Vol O2 Time of Stooping Energy Req Kneeling	Red Red 02 02 02 02 04 EXPi EXPi EXPi	

Code: U11-E9-R11 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 7:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 11: 0.01394 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 9: 2000 cal/min (140 Watts)

equired	2	• 🕶	œί	83,78	25,00	3.47	1.94	0.63		•	1.		93.90	1.31	1,94	•	0.56	28,50	8,10	49.00	ij	3484.49	1942.18	25.98	œ,	14.48
oxygen required	w	, C	2.8	83.78	υ.	3.47	1.94	0.63	ö		.	v.		1.31	1.94	1.00	0.56	28.50	8.10	20.02	6644.90	8533, 45	4756.35	<u>ب</u>	6.82	œ.
s/ lpm of	ທ	Sanding	'n	83.78	ö	•	1.51	•		139.47		45.57		1.31	1.94	1.29	0.72	26.50	4.40	33.00	Q	1981.23		7.96	6.64	
1.74 watts/	4		ζ.	•	21.00		2.11	0.66	٥.		71.94	ζ.	92.19		1.94	0.92		28.50	8.10	20.00		1422.18	792.69	+	3.68	ω.
11: 7	m	Painting	80.	81.77	6.0	3,36	•	0.62		4	1.9	۲.	94.75	1.32	1.94	1.03	0.58	26.50	4.40	48.00	2471.49	2881.85	2061.13	æ	5.69	ω.
n Reference	(V	<u>-</u>	ò	۲.	را د.	₹.	1.94	0.63	0		71.94		•	1.31		•	0.56	28.50	8.10		3267.08	4195.61	2338,54	4.54	3.25	ທຸ
mated from	4			83.78	25.00	3.47	1.94	0.63	2000.00	139.47	71.74	45.44	94.03	1.31	1.94		0.56	26.50	4.40	55.00	2834.51	3305.15	2363.88	11.22	9.36	
Rate esti		Units	E	k g	gears	l par	l pm		cal/min	Watts	watt/1pm	Watts	Watts	lpm	lpm	×	×	te 02	-/+	ain	liters			mq/m/3	mg/m/3	mg/m/3
Basal Metabolic Rate esti	Sample #	Operation	Height	Weight	Age	Vol Rate 02 (max)	Vol Rate 02 (AI)	Vol Rate 02 (0 Watts)	Total Energy Req	Total Energy Req	Std Metabolism	Basal Rate	Energy Reg (work)	Vol Rate O2 (Work)	Total Rate O2 Req	% of AT Required	% of Vol 02 (max)	Val Rate Expir/Vol Rate	Vol Expir/Vol 02	Time of Work	Total Vol Exp (Ave)	Total Vol Exp (Max)	Total Vol Exp (Min)	Conc (min)	Conc (ave)	Conc (max)

Code: U11-E9-R6 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 8:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 11: 0.01394 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 9: 2000 cal/min (140 Watts)

•	•	۲.	3.44	•	•	8.09	mg/m/3	Conc (max)
22.18	8.14	7.92	4	6.29	3.88	10.39	mg/m/3	Conc (ave)
	11.37	4	6.18	•	•	5.	mg/m/3	Conc (min)
1627.94	3986.79	1187.73	659.65	1600.50	1960.17	1827.28		Total Vol Exp (Min)
2920.71	<u>ر</u>	1660.67	4	œ	51	Ω.		Total Vol Exp (Max)
2274.33	5569.78	424.	21.5	2235.99	38.4	2552.82	liters	Total Vol Exp (Ave)
റ്	0.0	33.00	•	4	59.0	55.00	ri e	Time of Work
8.10	m.	4.40	•	8.10	•		-/+	Vol Expir/Vol 02
28.50	•	26.50	ហ		28.50	28.50	ite 02	Vol Rate Expir/Vol Rate
0.47		ö	0.43	0.49	•	0.47		% of Vol 02 (max)
0.84	•	1.08	•	œ	0.84		×	% of AT Required
1.63	1.63	•	1.62	1.63	•	•	l pa	Total Rate O2 Req
1.00	1.00	1.00	0.96	1.01	1.00	1.00	l pa	Vol Rate O2 (Work)
71.35	_	71.35	68.81	۰.	71.35	71.35	Watts	Energy Req (work)
68.11			70.65	66.84	68.11	68.11	Watts	Basal Rate
107.53			107.53	ທຸ	107.53	107.53	watt/lpm	Std Metabolism
139.47	139.47	139.47	139.47	139.47	139.47	139.47	Watts	Total Energy Req
	2000.00		2000.00		2000.00	2000.00	cal/win	Total Energy Red
0.63	0.63	0.63	0.66	0.62	0.63	0.63		Vol Rate OZ (O Watts)
1.94	•	1.51	2.11	1.88	1.94	•		Vol Rate 02 (AI)
3.47	3.47	5.69	3.77	3,36	3.47	3.47	l p.m.	Vol Rate 02 (max)
	25.00	50.00	•	26.00	25.00	25.00	years	Age
83.78	83.78	ω	87.79	81.77		83.78	Kg	Weight
182.88		182.88	•	m.	ġ	٠i	E 0	Height
Sanding	Sanding	Sanding	Painting	Painting	Sanding	Sanding	Units	Operation
۲-	9	ស	4	m	2	4		

Code: 1/11-E9-R12 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 9:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 11: 0.01394 |pm O2/watt Ergonomic Estimate of Total Energy Required from Reference 9: 2000 cal/min (140 Watts) Racal Motabolic Date estimated from Peteronce 12: See Table S

Basal Metabolic Rate estim	Rate estima	ated from	Reference	e 12: See	e Table S	•		
Sample #		4	2	ю	4	ហ	9	~
Operation	Units	. ~	Sanding	ing	Painting	Sanding	Sanding	_
Height	Ę	182.88	182.88	180.34	Ÿ.	182.88	182.88	182.88
Weight	X Q	83.78	83.78	81.77	ζ.	83.78	ю	83.78
Age	gears	25.00	25.00	26.00	21.00	50.00	25.00	25.00
Vol Rate 02 (max)	lpm.	3.47	3,47	3.36	•	2.69	3.47	3.47
Vol Rate 02 (AT)	l par	1.94	1.94	1.88	2.11	1.51	1.94	1.94
Vol Rate 02 (0 Watts)		0.63	0.63	0.62	•	_•	0.63	0.63
Total Energy Req	cal/min	•	2000,00	2000.00	2000.00	2000.00	2000.00	2000.00
Total Energy Req	Watts	139.47	139.47	139.47	139.47	139.47		139.47
Std Metabolism	cal/m^2/hr	40.24	40.24			40.24	40.24	40.24
Basal Rate	Watts	0.10	0.10	0.09	0.10	0.10	0.10	0.10
Energy Reg (work)	Watts		139,37	139.37	139.37	139.37	139.37	139.37
Vol Rate O2 (Work)	l pm	1.94	•	1.94	1.94		1.94	1.94
Total Rate O2 Req	md [•	•	•	2.60	2.58		2.58
% of AT Required	×	1.33	1.33	1.36	•	1.71	1.33	1.33
% of Vol 02 (max)	×	•		0.76	0.69	0.96	0.74	0.74
	Rate 02	26.50	26.50	26.50	26.50	26.50	26.50	26.50
Vol Expir/Vol 02	-/+	4.40	4.40	4.40	4.40	4.40	4.40	4.40
Time of Work	C1 E	55.00	59.00	48.00	20.00	33.00	120.00	49.00
Total Vol Exp (Ave)	liters	3756.22	4029.40	3263.16	1378.40	2253.73	8195.40	3346.45
Total Vol Exp (Max)		4379.90	4698.44	3804.97	1607.26	2627.94	9556.14	3902.09
Total Vol Exp (Min)		3132.55	3360.37	2721.35	1149.53	1879.53	6834.65	2790.82
Conc (min)	E/m/6m				3.54	6.00		18.08
Conc (ave)	mg/m/3	7.06	2.64	4.31	5.96	5.00	5.53	15.08
Conc (max)	mg/m/3	•					•	12.93

Code: U6-E8-R11 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 10:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 6: 0.0093 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 8: 3400 cal/min (238 Watts) Basal Metabolic Rate estimated from Reference 11: 71.74 watts/ lpm of oxygen required

~	Sanding	182.88	83.78	25.00	3.47	1.94	0.63	•	237.09		45.57	191.52	1.78		1.24	0.70	26.50	4.40	49.00	in.	3655.92	2614.75	19.30	16.09	13.80
9	Sanding	182.88	83.78	25.00	•	1.94	•	3400.00	237.09	•	45.57	191.52	•	2.41	•	•	26.50	4.40	120.00	7678.38	8953.28	6403.48	•	5.91	•
ហ		182.88	83.78	50.00	5.69	1.51	•	3400.00	237.09	•	45.57	191.52	٠	2.41	1.60	•	26.50	4.40	33.00	. S	2462.15	6.0	6.40	5.34	•
4		187.96		21.00	•	2.11	0.66	3400.00	237.09		47.27	189.82	•	•	1.15		26.50	4.40	20.00	1283.88	1497.05	1070.70	œ.	3.17	~
m		180.34	81.77	26.00	3,36	1.88	0.62	3400.00			44.72	•	1.79	•	1.28	•	26.50	4.40	48.00	3066.38	3575,51	2557.24	5.50	4.59	
~	nding	182.88	83.78	25.00	3.47	•	0.63	3400.00	•		45.57	•	•	2.41	1.24	•	26.50	4.40	59.00	3775.20	4402.03	3148.38	•	2.81	4
₽	Sanding	'n	83.78	25.00	3.47	1.94		3400.00	237.09	71.74	_	191.65		2.42	•	•	26.50	4.40	55.00	3521.03	4105.65	2936.40	•	7.53	•
	Units	E	λ g	years	lpm	l per	~	cal/min	Watts	watt/lpm	Watts	Watts	Pw Tbw	l pm	ж.	×		-/+	Bir	liters			mg/m/3	mg/m/3	mg/m/3
Sample #	Operation	Height	Weight	Age	Vol Rate 02 (max)	Vol Rate 02 (AI)	Vol Rate 02 (O Watts)	Total Energy Req			Basal Rate	Energy Red (work)	Vol Rate 02 (Work)	Total Rate 02 Req	% of AT Required	% of Vol 02 (max)	Vol Rate Expir/Vol Rate	Vol Expir/Vol 02	Time of Work	fotal Vol Exp (Ave)	Total Vol Exp (Max)	Total Vol Exp (Min)	Conc (min)	Conc (ave)	Conc (max)

Code: U6-E8-R6 Dust/Mist Sampling Results for Respirator Flow Model # 11: Appendix III:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 6: 0.0093 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 8: 3400 cal/min (238 Watts) Basal Metabolic Rate estimated from Reference 6: 107.53 watts/ lpm of oxugen required

1 2 3 nding Sanding Painting Pa	1 2 3 ing Sanding Painting Pa	2 ing Painting Pa	3 inting Pa	10	+'	5 Sanding	ndi	
182.88 182.88 180.34	.88 182.88 180.34	82.88 180.34	80.34	• 1	187.96		182.88	182,88
83.78 25.00	5.00 25.00 26.	3.78 81. 5.00 26.	81.77 26.00		\sim \leftarrow	83.78 50.00	83.78 25.00	25.8
3.47 3.47 3.	47 3.47 3.	.47 3.			3.77	2.69	3.47	3,47
1.94 1.94 1.	94 1.94 1.	.94 1.	1.88		•	1.51	1.94	1.94
0.63	63 0.63 0.	.63 0.	0.62		0.66	0.63	0.63	0.63
3.00 3400.00 3400.	.00 3400.00 3400.	00.00 3400.	400.		3400.00	3400.00	_	3400.00
237.09 237.09 237.	7.09 237.09 237.	37.09 237.	-		237.09	237.09	-	237.09
7.53 107.53	7.53 107.53 107.	07.53 107.	_		107.53	107.53	-	107,53
68.11 68.11 65.	1 68.11 65.	.11 65.	-		70.65	68.11	68.11	68.11
B 168.98 170.	B 168.98 170.	.98 170.	-	ហ	166.44		_	168.98
7 1.57 1.5	7 1.57 1.5	.57 1.5	ı.	m	1.55	1.57		1.57
2.20 2.20 2.2	.20 2.20 2.2	.20 2.2	ú	Q	2.20	2.20	2.20	2.20
.13 1.13 1.	.13 1.13 1.	.13 1,		2	•			•
.63 0.63 0.	.63 0.63 0.	.63 0.	•	يو	0.58	0.82		0.63
26,	.50 26.50 26.	6.50 26.	•	S S	26.50	26.50	26.50	26.50
+/ 4.40 4.40 4,	.40 4.40 4.	.40 4.	•	40	4.40	4.40	4.40	4,40
.00 48.	5.00 59.00 48.	.00 48.		90	20.00	33.00	120.00	49.00
.73 3447.45 28	.73 3447.45 2804.	.45 2804.	٠.	-	1168.63	1928.24	7011.76	2863.14
.86 3270.3	.33 4019.86 3270.3	.86 3270.3	(Li	6	1362.66	2248.40	8175.98	3338,53
2680.13 2875.04 2339.02	.13 2875.04 2339.0	75.04 2339.0	339.0		974.59	1608.08	5847.55	2387,75
9.90 3.70	90 3.70 6.	.70 6.			•	7.01	۲.	21.13
8.25 3.08 5.	25 3.08 5.	.08 5.			3.49	5.85	6.47	17.62
7.08 2.64	08 2.64 4.	.64 4.			•	5.05	ĸ.	, 1

Code: U6-E8-R12 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 12:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 6: 0.0093 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 8: 3400 cal/min (238 Watts) Basal Metabolic Rate estimated from Peference 12: See Table 5.

6	Sandi	8 182.88	8 83.78		~	4 1.94	_	0 3400.00	23	4 40.24	0.10	0 237.00	0 2.20	4 2.84	₩.	_	0 26.50	0 4.40	0 49.00	4 3684.49	4 4296.26	4 3072.73	Ŧ	13.6	1 11.74
_	Sanding	'n	83.78	25.00	3.4	1.9	0.63	3400.00	237.09	40.24	0.1	237.0	2.2	2.84	1.4	•	26.5	4.40	120.00	9023.2	10521.4	7525.0		5.03	m,
ហ	Sanding	182.88	83.78	50.00	2.69	1.51	0.63	3400.00	237.09	40.24	0.10	237.00	2.20		•	1.05	•	6.90	33.00	3530.13	4176.23	2884.03		3.19	
4	Painting	187.96	Ķ	21.00	•	2.11	•	3400.00	237.09	40.24	•	236.99	•	2.86	•	0.76	26.50	4.40	20.00	1516.38	1768.16	1264.61		2.69	
m	ing	180.34	81.77	26.00	3.36	1.88	0.62	3400.00	237.09	40.24	0.09	237.00	2.20		1.50	0.84	26.50	4.40	48.00	3594,29	4191.07	2997.50	9.	3.91	\mathfrak{C}
2		182.88	83,78	25.00	3,47	1.94	0.63	3400.00	237.09	40.24	0.10	237,00	2.20	2.84	1.46	0.82	26,50	4,40	59,00	4436.43	5173.04	3699.81		2.39	
Ħ	Sanding	ď	83.78	25.00	3.47	1.94	0.63	3400.00	237.09	40.24	0.10	•	•	2.84	•	•	26.50	4.40	55.00	4135.65	4822.33	3448.98	•	6.41	5.50
	Units	eo	ر 0	sueah	Ipa	Ipm		cal/min	Watts	cal/m^2/hr	Watts	Watts	Ipm	I pa	.×	×	ste 02	-/+	ain nie	liters			mg/m/3	mg/m/3	mg/m/3
Sample #	Operation	Height	Weight	Age	Vol Rate 02 (max)	Vol Rate 02 (AT)	Vol Rate 02 (0 Watts)	Total Energy Req	Total Energy Req	Std Metabolism	Basal Rate	Energy Red (work)	Vol Rate 02 (Work)	Total Rate 02 Req	% of AT Required	% of Vol 02 (max)	Vol Rate Expir/Vol Rate	Val Expir/Val 02	Time of Work	Total Vol Exp (Ave)	Total Vol Exp (Max)	Total Vol Exp (Min)	Conc (min)	Conc (ave)	Conc (max)

Code: U6-E10-R11 Dust/Mist Sampling Results for Respirator Flow Model # 13: Appendix III:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 6: 0.0093 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 10: See Table 4. Basal Metabolic Rate estimated from Reference 11: 71.4 watts/ lpm of oxygen required

;	Sanding 182 88	83.7	0	4	σ	Ý		98.	+	'n.	ω		•			26.50	•	•	2550.00	77.8	107.53	3.1	٧.٧	Ö	٦.	4	ø.	ហ	4	6.00 PAGE
;	Sanding	83.7	5.0	3.4	0.	9.	50.0	198.7	1.7	5.4	153.32	4	٥.	0	'n	Ŋ.	4.40	20.00	50.0	177.8	07	3.1	۶.۷	•	۲.	٦.	φ.	ĸ.	4	$\circ \times$
	ט ס	83.7	0.0	2.6	S.	9.	0.0	98.7	1.7	5.4	S	4	٥.	m.	۲.	ιŪ.	4.40	0	50.0	7.8	107.53	8.1	9.7	0		4	œ	ល	4	o.⊋
	Painting 187 of	87.7	1.0	3.7	7	9.	50.0	142.9	1.7	7.1	95.84	æ	S.	۲.	4.		۲.	0.	1750.00	2.0	07	9.0	1.3	4.	ო.	9.	ო.	28.50	۲.	00
ო :	Painting 180 24	81.7	6.0	(i)	ໝ	Ψ.	50.0	142.9	1.7	5.5	98.38	σ.	ល	α	4	28.50	٦.	41.00	1750.00	2.0	07	6.8	5.1	ທຸ	m.	۲.	4.	ທຸ	8.10	0.00
∾:	ding ag	83.7	S.0	3.4	9	9.	50.0	۲.	1.7	5.4	153.32	4	0.	0.	ល	ທ	4	٥.	50.0	77.8	107.53	B. 1	9.7	0	۲.	۲.	9.	'n	4	
	ם מ	83.7	0.0	4.6	6.	9.	0.0	98.7	1.7	7. 4	ω	4	0	0	s.	ស	4	42.00	50.0	177.8	107.53	+	۲.	0	۲.	۲.	9	ù	4	
	Ę	אר ק פ	Lears] Ipm	. To	. Fd	cal/min	Watts	watt/1pm	Watts	Watts	l pm	lp.	. ×	×		-/+	e in	cal/min	Watts	watt/1pm	Watts	Watts	lpm	lpa mdl	×	×		-/+	Ē
Sample #	Operation		Age	Vol 02 (max)	Anerobic Threshold	Vol G2 (O Watts)	Energy Reg Standing	Req Standing	letabolism _	Basal Rate	Energy Red (work)	Vol O2 (Wark)	Total O2 Required	% of AT Required	% of Vol 02 (max)	Vol Expir/Vol 02	Vol Expir/Val 02	Time of Standing	Energy Reg Sitting	Energy Reg Sitting		Basal Rate	Energy Req (work)	Vol 02 (Work)	Total O2 Required	% of AT Required	% of Vol 02 (max)		Vol Expir/Val O2	Time of Sitting

(can't) Dust/Mist Sampling Results for Respirator Flow Model # 13: Appendix 111:

7 Sanding	3050.00 212.69 107.53 68.11 144.57 1.34 2.65 2.65 1.36 0.76 4.40	2750.00 191.77 107.53 68.11 123.65 1.15 2.36 1.21 0.68 26.50 4.40	2848.88 3321.91 2375.86 18.95 15.80
6 S an ding	3050.00 212.69 107.53 68.11 144.57 1.34 2.65 1.36 0.76 26.50 4.40	2750.00 191.77 107.53 68.11 123.65 1.15 2.36 1.21 0.68 26.50 4.40	6023.67 7023.82 5023.51 8.00 6.67 5.72
5 Sanding	3050.00 212.69 107.53 68.11 144.57 1.34 2.65 1.76 0.98 26.50 4.40	2750.00 191.77 107.53 68.11 123.65 1.15 2.36 1.56 0.88 26.50 4.40	1877.53 2189.27 1565.79 3.83 3.19
4 Painting	2250.00 156.90 107.53 70.65 86.25 0.80 1.86 0.88 0.49 28.50 81.10	1950.00 135.98 107.53 70.65 65.35 0.61 1.57 0.74 0.74 0.74 0.74	882.58 1133.41 631.74 6.45 4.62
3 Painting 1	2250.00 156.90 107.53 66.84 90.06 0.84 1.88 1.00 2.85 28.50 8.10	1950.00 135.98 107.53 66.84 69.14 0.64 1.59 0.84 0.47 28.50 8.10	2170.06 2786.82 1553.31 9.05 6.43
2 Sanding	3050.00 212.69 107.53 68.11 144.57 1.34 2.65 1.36 2.65 1.36 0.76 26.50 4.40	2750.00 191.77 107.53 68.11 123.65 1.15 2.36 1.21 0.68 26.50 4.40	3235.57 3772.80 2698.34 3.94 3.28
1 Sanding	3050.00 212.69 107.53 68.11 144.57 1.34 2.65 1.36 0.76 26.50 4.40	2750.00 191.77 107.53 68.11 123.65 1.15 2.36 1.21 0.68 26.50 4.40	3094.04 3607.77 2580.31 10.28 8.57 7.35
	cal/min Watts watt/lpm Watts Watts Ipm Ipm 1,2,2,2,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,	cal/min Watts watt/lpm Watts Ipm lpm // // // // // // // // // // // // //	liters mg/m/3 mg/m/3 mg/m/3
Sample # Operation	Energy Req Stooping Std Metabolism Basal Rate Energy Req (work) Vol 02 (work) Total 02 Required % of AT Required % of AT Required % of Wol 02 (max) Vol Expir/Vol 02 Vol Expir/Vol 02 Time of Stooping	Energy Req Kneeling Std Metabolism Basal Rate Energy Req (work) Vol O2 (Work) Total O2 Required % of AT Required % of Wol O2 (max) Vol Expir/Vol O2 Vol Expir/Vol O2	Vol Exp (Ave) Vol Exp (Max) Vol Exp (Mir) Conc (min) Conc (ave)

Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 14: Code: V6-E10-R6

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 6: 0.0093 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 10: See Table 4. Basal Metabolic Rate estimated from Reference 6: 107.53 watts/ lpm of oxygen required

-	2	Sanding	œ.	~	Ö	4		Ψ,		50.0	8.7	07.5	8.1	9.0	3	œ	σ.	ຫຸ	28,50			50.0	177	1.7	5.4	2.4	Ġ	4	Ġ	۲.	ហ៊		0.9	PAGE
ו	ω	Sanding	œ	<u>.</u>	Ō.	4	Q.	9.	,	50.0	8.7	07.5	8.1	9.0	3	œ	Ø.	ß.	28.50	۲.	0.	50.0		1.7	7.4	2.4	Ġ	4	ä	۲.	Ŋ.	4	Õ	ON NEXT
-	ហ	Sanding	85.8	3.7	0.0	9	ហ	9.		50.0	8.7	07.5	8.1	9.0	0	œ	ς.	9	26.50	4		50.0	-	۲.	5.4	2.4	Š	4	9.	σ.	ល	4.40	8.00	CONTINUED
	4	Painting	87.9	7.7	1.0	۲.	₩.	9.		0.0	42.9	S.	9.0	2.3	9.	ω.	9.	æ.	28.50	٠,	0.	50	122.03	1.7	7.1	4.9	۲.	۲.	Φ.	4.	S.	٦.	0.	
	e	σ.	80.3	۲.	0.	m	œ	9		0.0	2.9	07.5	6.8	6.1	۲.	Ġ,	۲.	4	28.50	٠,	Ō.	50.0	122.03	1.7	4.5	7.4	۲.	۲.	σ,		R)		٥.	
	2	Sanding	82.8	3.7	5.0	4	σ.	φ.	1	50.0	98.7	ιù	8.1	9.0		ω.	σ,	ល	28.50		٥.	50.0	177.82	1.7	5.4	2.4	3	4	Ŋ	۲.	ı.		0.	
	~	Sanding	82.8	ы У	0.0	4.	σ.	9.	,	0.0	8.7	07.5	8.1	9.0	Ġ	ω.	σ.	ī.	28.50	. 1	٥.	50.0	177.82	1.7	5.4	2.4	Ġ	4	Ġ	۲.	ល	4	٥.	
			E O	A O	years	lρω	nd!	lpa		cal/min	Watts	watt/lpm	Watts	Watts	lpm	lpm	х.	×		-/+	c i e	cal/min	Watts	watt/lpm	Watts	Watts	lpm	lpm	×	×		-/+	n i n	
	Sample #	Operation	Height	Weight	Age	Ual 02 (max)	Anerobic Threshold	Uol O2 (0 Watts)		Energy Req Standing	Energy Req Standing		Basal Rate	Energy Req (work)	Vol 02 (Work)	Total P2 Required	% of AT Required	% of Vol O2 (max)	Vol Expir/Vol 02	Vol Expir/Vol 02	Time of Standing	Energy Reg Sitting	Energy Req Sitting	bolism	Basal Rate	Energy Reg (work)	Vol O2 (Work)	Total O2 Required	% of AT Required	% of Vol 82 (max)	Vol Expir/Vol 02	Vol Expir/Vol 02	Time of Sitting	

(can't) Dust/Mist Sampling Results for Respirator Flow Model # 14: Appendix III:

7 Sandirig	3050.00 212.69 71.70 45.42 167.27 1.56 2.97 1.53 0.85 26.50 4.40	2750.00 191.77 71.70 45.42 146.35 1.36 2.67 1.38 0.77 26.50 4.40	3023.33 3668.49 2378.17 18.93 14.89
6 Sanding	3050.00 212.69 71.70 45.42 167.27 1.56 2.97 1.53 0.85 26.00	2750.00 191.77 71.70 45.42 146.35 1.36 2.67 1.38 0.77 26.50 4.40	6356.59 7723.27 4989.92 8.05 6.32
5 Sanding	3050.00 212.69 71.70 45.42 167.27 1.56 2.97 1.97 1.10 37.70 6.90	2750.00 191.77 71.70 45.42 146.35 1.36 2.67 1.77 0.99 26.50 4.40	1799.21 2097.95 1500.48 4.00 3.33 2.86
4 Painting	2250.00 156.90 71.70 47.11 109.79 1.02 2.19 1.04 0.58 26.50 4.40	1950.00 135.98 71.70 47.11 88.87 0.83 1.90 0.90 0.50 28.50 8.10	757.79 973.16 542.42 7.51 5.38
3 Painting	2250.00 156.90 71.70 44.57 112.33 1.04 2.19 1.16 0.65 26.50 4.40	1950.00 135.98 71.70 44.57 91.41 0.85 1.90 1.01 0.56 26.50 4.40	1959.39 2468.30 1450.48 9.70 7.18 5.70
2 Sanding	3050.00 212.69 71.70 45.42 167.27 1.56 2.97 1.53 0.85 26.50 4.40	2750.00 191.77 71.70 45.42 146.35 1.36 2.67 1.38 0.77 26.50 4.40	3144.27 4021.15 2267.38 4.69 3.38 2.64
1 Sanding	3050.00 212.69 71.70 45.42 167.27 1.56 2.97 1.53 0.85 26.50 4.40	2750.00 191.77 71.70 45.42 146.35 1.36 2.67 1.38 0.77 26.50 4.40	3123.43 3903.48 2343.38 11.32 8.49 6.79
	cal/min Watts watt/lpm Watts Watts Ipm Ipm 1pm 1pm 1pm	cal/min Watts watt/lpm Watts lpm lpm // // // // // // // // // // // // //	liters mg/m/3 mg/m/3 mg/m/3
Sample # Operation	Energy Req Stooping Std Metabolism Basal Rate Energy Req (work) Vol 02 (Work) Total 02 Required % of AT Required % of Ol 02 (max) Vol Expir/Vol 02 Vol Expir/Vol 02	Energy Req Kneeling Std Metabolism Basal Rate Energy Req (work) Vol 02 (Work) Total 02 Required % of AT Required % of AT Required % of Expir/Vol 02 Vol Expir/Vol 02 Jol Expir/Vol 02	Uol Exp (Ave) Uol Exp (Max) Uol Exp (Min) Conc (min) Conc (ave) Conc (max)

Code: U6-E10-R12 Appendix III: Dust/Mist Sampling Results for Respirator Flow Nodel # 15:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 6: 0.0093 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 10: See Table 4. Basal Metabolic Rate estimated from Reference 12: See Table 5.

Sample #		4	7	ო	4	ហ	φ	2
Operation		Sanding	Sanding	ב	٠ <u></u> ا	Sanding		Sanding
Height	EO	82.	82.	8	87.9		82.	82.8
Weight	X Q		ю Э		۲.		•	3.7
Age	years	ю	'n.		1.0		ů,	S.0
Uol 02 (max)	Ed!	•	•		۲.		٠	4.
Anarobic Threshold	Ed.	•	1.94		۲.		1.94	σ.
Vol O2 (0 Watts)	lpm	•	•		9.		•	9
Energy Reg Standing	cal/min	2850.00	2850,00	2050.00	2050.00	2850.00	2850.00	0
	Watts	198.74	98.	142.95	Ŋ.	198.74	m.	198.74
letal	cal/m^2/hr	8	40.24	40.24	9.2		o.	'n
Basal Rate	Watts	•	0.10		۲.		0.10	٠,
Energy Req (work)	Watts		•	•	142.85	•	•	9
Vol O2 (Work)	l pm	1.85	1.85	1.33	1.33	1.85	1.85	1.85
Total O2 Required	I eq		•	•	φ.		•	4
% of AT Required	×	•	•	•	σ.	•	•	Š
% of Vol O2 (max)	×	•			0.53		•	۲.
Vol Expir/Vol 02		26.50	26.50	26.50	28.50	26.50	26.50	26.50
	-/+	4.40		4.40	B.10	•	4.40	4.40
Time of Standing	nin	45.00	57.00	41.00	20.00	26.00	50,00	23.00
Energy Reg Sitting	cal/min	50.0		1750.00	1750.00		2550.00	50.0
Energy Req Sitting	Watts	•	. •	122.03	22.0	177.82	177.82	177.82
Std Metabolism	cal/m^2/hr	40.2	0.2	40.24	0.2		ö	Ŋ
Basal Rate	Watts	0.10	0.10	_•	0.10	•	0.10	0.10
Energy Req (work)	Watts	۲.	177.72	121.94	121.93	•	. •	^.
Vol O2 (Work)	l pm	1.65	φ.	٦.	. 1	1.65	•	1.65
Total O2 Required	l pa	٠,	٠,	2.32	2.36	•	3.11	٠,
% of AT Required	×	9	9	ď	٦.	•	•	٠.
% of Vol 02 (max)	×	ი.	σ.	9.	9	•	•	σ.
Vol Expir/Vol 02		ĸ.	26.50	٠	26.50		26.50	26.50
Vol Expir/Vol 02	-/+	4	4.40	4.40	4.	6.90	•	4
Time of Sitting	CIE	2.00	0.00			8.00	18.00	6.00
					_	CONT INUED	ON NEXT	PPIGE

(con't) Dust/Mist Sampling Results for Respirator Flow Model # 15: Appendix III:

7 Sanding	3050.00 212.69 40.24 0.10 212.59 1.98 3.60 1.85	. 60	2750.00 191.77 40.24 0.10 191.67 1.78 3.31 1.70 0.95 26.50 4.40 20.00 3759.36 4383.55 3135.16	14.36 11.97 10.27
6 Sanding	3050.00 212.69 40.24 0.10 212.59 1.98 3.60 1.85	. o o	2750.00 191.77 40.24 0.10 191.67 1.78 3.31 1.70 0.95 26.50 7.00 8911.99 10451.63	5.45 4.51 3.84
5 Sanding	3050.00 212.69 40.24 0.10 212.59 1.98 3.60 2.39	.00	2750.00 191.77 40.24 0.10 191.67 1.78 3.31 2.19 1.23 37.70 6.90 0.00	2.27 1.93
4 Painting	2250.00 156.90 40.24 0.10 156.80 1.46 2.84 1.35	4.0	1950.00 135.98 40.24 0.10 135.88 1.26 2.55 26.50 4.40 0.00 1131.79 1453.46 810.13	5.03 3.60 2.80
3 Painting (2250.00 156.90 40.24 0.09 156.80 1.46 2.81 1.49 0.84	4.V.	1950.00 135.98 40.24 0.09 135.88 1.26 2.52 2.52 1.34 0.75 26.50 4.40 0.00 2639.87 3078.19	6.39 5.33 4.57
2 Sanding l	3050.00 212.69 40.24 0.10 212.59 1.98 3.60 1.85	0.0	2750.00 191.77 40.24 0.10 191.67 1.78 3.31 1.70 0.95 26.50 2.00 2.00 3271.23	3.25 2.71 2.32
1 Sanding	3050.00 212.69 40.24 0.10 212.59 1.98 3.60 1.85	.0.0	2750.00 191.77 40.24 0.10 191.67 1.78 3.31 1.70 0.95 26.50 4.40 11.00 3889.95 4535.83	8.17 6.82 5.85
	cal/min Watts cal/m^2/hr Watts Watts Ipm Ipm	+/- cie	cal/min Watts Watts Watts Watts Ipm 1pm 1pm 1pm 1pm 1pm 1pm 1pm 1pm	E/#/6# E/#/6#
Sample # Operation	Energy Req Stooping Std Metabolism Std Metabolism Basal Rate Energy Req (work) Vol O2 (Work) Total O2 Required % of AT Required % of Vol O2 (max)	Vol Expir/Vol 02 Vol Expir/Vol 02 Time of Stooping	Energy Req Kneeling Std Metabolism Basal Rate Energy Req (work) Vol 02 (Work) Vol 02 (Work) Total 02 Required % of AT Required % of AT Required % of Ol 02 (max) Vol Expir/Vol 02 Vol Expir/Vol 02 Time of Stooping Vol Exp (Ave) Vol Exp (Max)	Conc (min) Conc (ave) Conc (max)

Code: U6-E9-R11 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 16:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 6: 0.0093 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 9: 2000 cal/min (140 Watts) Basal Metabolic Rate estimated from Reference 11: 71.74 watts/ lpm of oxygen required

Sample #	! 4 .,	₩ (N	9				٠,
	Units	Sanding 182,88	Sandıng 182.88		Fainting 187.96	5anding 182.88	3and1ng 182.88	5and1ng 182.88
	אַס	83.78	83.		87.78	83.78		83.78
	years	25.00	25.00	26.00	21.00	50.00	25.00	25.00
	I pa	3.47	3.47	3.36	•	2.69	3.47	3.47
	lp.	1.94	1.94	1.88	2.11	1.51	1.94	1.94
Vol Rate O2 (0 Watts)	l pa	0.63	0.63	0.62	0.66	0.63	0.63	0.63
Ü	cal/min	2000.00	0	2000.00	2000.00	•	•	2000.00
	Watts	139.47	139.47		139.47	139.47	139.47	139.47
3	watt/1pm	71.74	71.94	71.94	71.94	71.94		•
	Watts	45.44	45.57		47.27	45.57	45.57	45.57
	Watts				92.19			93.90
	l pm	•	0.87	0.88	0.86	0.87	0.87	_•
	l pm	1.51	1.51	1.50	1.51	1.51	1.51	1.51
	×	•	0.77	08.0	0.72	•	0.77	0.77
	×	0.43	0.43	0.45	0.40	0.56	0.43	0.43
Vol Rate Expir/Vol Rate	02	28.50	28.50	28.50	28.50	28.50	28.50	28.50
	-/+	8.10	8.10	8.10	8.10	8.10	8.10	8.10
	nie Cie	55.00	59.00	48.00	20.00	33.00	120.00	49.00
_	iters	2363.60	2533, 45	۲,	863.26	1417.01	5152.78	2104.05
		3035.35	3253.48	2640,03	1108.60	1819.74	6617.25	2702.04
		1691.84	1813.42	1471.49	617.91	1014.28	3688.30	1506.06
E	mg/m/3	•				11.12	12.29	33.50
€	mg/m/3	11.22	4.19	6.84	4.72	7.96	•	•
E	mg/m/3	•	•		•	6.20	6.85	18.67

Cade: U6-E9-R6 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 17:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 6: 0.0093 lpm G2/watt Ergonomic Estimate of Total Energy Required from Reference 9: 2000 cal/min (140 Watts) Basal Metabolic Rate estimated from Reference 6: 107.53 watts/ 1pm of oxygen required

	2	Sanding	182.88	ю	'n	•	1.94	0.63	_	_	107.53	_	_	0.66	1.30	0.67	0.37	28.50	8.10	49.00	811.	٠.	N	φ. φ.	27.86	1.6
ת ת	Q	. 🕶	'n	83.78	Ŋ.	•	1.94	0.63	•	•	107.53	•	•	0.66	•	0.67	•	28.50	8.10	120.00	432.B	5696.57	₩.		10.22	σ.
	ល	ī	'n	•	ö	•	1.51		•				•	•	•	•	•	28.50	8.10	33.00	19.	566.	873.16	•	9.24	•
	4	.=	ζ.	•	7	•	2.11	•			107.53		68.81	0.64	•	•		28.50	8.10	20.00	739.31	949.43	529.19	~	5.51	Ň
) •	ന		·		•	3.36	1.88	0.62	2000.00		107.53			0.68	1.30	0.69	0.39		8.10	•	774.3	278.6	1270.06		7.93	
	N	Sanding	$\dot{\circ}$	•	Ŋ.	•	•	0.63			107.53		71.35	•	1.30		0.37	•	8.10	59.00	180.	æ.	1561.11	æ	4.87	۲.
	#1		182.88				1.94							0.66				28.50	8.10	Ξ.	33.1	610.	•	•	13.04	
; ; ;		Units	e 0	ķg	gears	l pa	Ipm		cal/min	Watts	watt/lpm	Watts	Watts	lpm	lpa md	×				nin	liters			mg/m/3	mg/m/3	m g/m/3
	Sample #	Operation	Height	Weight	Age	Vol Rate 02 (max)	Vol Rate O2 (AT)	Vol Rate 02 (0 Watts)	Total Energy Req	Total Energy Req		Basal Rate	Energy Red (work)	Vol Rate O2 (Work)	Total Rate 02 Req	% of AT Required	% of Vol 82 (max)	Vol Rate Expir/Vol Rate	Vol Expir/Vol 02	Time of Work	Total Vol Exp (Ave)	Total Vol Exp (Max)	Total Vol Exp (Min)	Conc (min)	Conc (ave)	Conc (max)

Code: U6-E9-R12 Appendix III: Dust/Mist Sampling Results for Respirator Flow Model # 18:

Increase Volume Rate of Oxygen per Increase in Work Rate From Ref 6: 0.0093 lpm O2/watt Ergonomic Estimate of Total Energy Required from Reference 9: 2000 cal/min (140 Watts) Basal Metabolic Rate estimated from Reference 12: See Table 5.

2	Ξ	'n	83.78	25.00		1.94		2000.00		•	0.10	139,37	1.30	1.93	•	•	•	8.10	49.	2694.65	3460.50	1928.80		18.72	14.58
9	\mathbf{c}	182.88	83.78	25.00	3.47	1.94	0.63	2000.00		40.24	•	139.37	1.30	•	•	0.56	28.50	8.10	120.00	6599.14	8474.69	4723.60		6.87	•
ស	C	'n	83.78	50.00	2.69	1.51	0.63	2000.00		40.24	0.10	139.37		1.93	•	•	26.50	4.40	33.00	687.4	1967.59	1407.24	•	6.68	•
4	t.		87.78	7	•	2.11	0.66	2000.00			0.10	139.37	•	1.95	•	•	28.50	8.10	20.00	113.3	1429.72	296.90	•	3.66	•
m	_	180.34	81.77	26.00	3.36	1.88	_•		•	40.24	0.03	139.37	•	1.92	•	•	•	4.40	48.00	2439.41	2844.44	2034.37		5.72	
2	nding	'n	83.78	25.00	•	1.94	•		•	40.24		139.37	1.30	1.93	•	•	28.50	8.10	59.00	3244,58	4166.72	2322,44	ທ	3.27	ທຸ
Ħ	٠,🛋	ė.	83.78	25.00	•	•		2000.00			0.10	139.37	1.30	1.93			•	8.10	55.00	24.	3884.23	2164.98	•	8.77	•
	Units	E	ح ح	Hears	lpa	. E C 7	_	Ö	Watts	cal/m^2/hr	Watts	Watts	lpm	l Da	۶.	*	ate 02		e.ie	liters			mq/m/3	mq/m/3	mg/m/3
Sagolo #	Operation	Height	Weight	Age	Uol Rate 02 (max)	Vol Rate 02 (AT)	Vol Rate 02 (0 Watts)	Total Energy Reg	Total Energy Reg	Std Metabolism	Basal Rate	Energy Reg (work)	Vol Rate 02 (Work)	Total Rate O2 Red	% of AT Required	% of Vol 02 (max)	Vol Rate Expir/Vol Rate	Vol Expir/Vol 02	Time of Work	Total Vol Exp (Ave)	Total Vol Exp (Max)	Vol Exp	Conc (min)	Canc (ave)	Conc (max)

Appendix IV

Organic Vapor Sampling Concentrations
by for Respirator Flow Model #17

Appendix IV: Organic Vapor Sampling Results by Concentration using Airflow Model # 17 for Respirator Cartridge Results

Time Sampled (min) Volume Sampled (m/3) Rethylcyclopentane n-Heptane Methylcyclohexane n-Octane 1,1,1-Trichloroethane Methyl Ethyl Ketone lsopropanol Trichloroethylene Toluene Ethluene Dichloride	#7 ¢	. 444040 4V	Resp (100-100-100-100-100-100-100-100-100-100	Cart U-1 m/3 m/3 5.D. /m/3 0.22 0.29 0.25 0.25 0.25 2.67 2.67 2.67 0.85 2.33 0.67	82.26 17.78 18.79 17.78 18.79 17.78 17.78 18.79 17.78	Sample 000-2 97 min 099 m/3 5.D. mg/m/3 .51 0.04 .72 0.03 .18 0.01 .42 0.03 .79 0.55 .79 0.55 .79 0.55 .79 0.55	Sesp Cart OU-2 56 min 2.170 m/3 0.30 0.0 0.73 0.0 1.56 0.2 11.46 1.9 8.58 0.7 12.49 1.0	esp Cart 00-2 56 min 170 m^3 30 0.03 73 0.07 56 0.26 60 0.10 58 0.70 58 0.70 58 0.70 65 0.46	82 Sample 100-3 48 mir 5.16 1.33 0.0 4.21 0.1 6.29 0.2 3.52 0.2 14.13 0.2 14.13 0.2 14.13 0.2	Sample 100-3 48 min 047 m^3 S.D. mg/m^3 .21 0.10 .29 0.16 .29 0.16 .52 0.28 .13 0.22 .66 0.56	Resp Cart 00-3 48 min 1.770 m/3 0.71 0.12 1.75 0.36 4.04 0.66 0.05 0.05 0.05 0.06 1.18 0.27 9.51 2.34 8.51 1.78	Sp Cart 00-3 48 min 770 m^3 5.D. mg/m^3 75 0.36 .04 0.60 .11 0.27 .51 2.34 .51 2.34
	1.70 6.33		1.86 8.45 3.42	0.21 0.94 0.38	3.50 9.82 4.95	0.23	2.52 8.47 4.37	0.25 1.03 1.46	2.50 0.06 0.80	0.00	0.00	0.00

Appendix IV: Organic Vapor Sampling Results by Concentration using Airflow Model # 17 for Respirator Cartridge Results (con't)

Cart S	e L	E < E	5.D. mg/m^3	1	0.03	0.08		1.64	9.15	0.21	96.9	1.45	2.16	0.33	0.18	0.51	0.13
Resp Cart OV-5	51	1.885	√6 ₪	•	0.11	0.32		10.74	8.44	1.46	30,10	10.52	18,01	2,22	1,50	4.18	0.52
Sample OU-5	min	6 √ e	S.D. mg/m^3	,	00.	0.01		0.08		0.05	8.48	0.18	0.19	0.15	0.02	0.10	0.07
82 Sam 00	51	0.053	<u> </u>	:	0.15	0.37		12.63		1.92	5.61	16.80	22.04	4.46	2.05	5.36	1.54
Cart -4	min Tin	E~E	G.D. mg/m^3		1.09	1.02	1.15						1.38		1.48		2.46
Resp Cart OV-4	23	0.850) Bu		2.21	6.18	10.31						26,45		2,17		0.48
р] e	min	8√₽	S.D. ጠ⊈/m^3	0.01	0.04	0.08	0.11	8.			0.21		0.52		0.08		0.02
BZ Sāmple OU-4	23	0.033) DE	0.46	2.67	9.36	9.56				2.50		39.60		3.51		0.93
	Time Sampled (min)	Volume Sampled (m^3)		İsopentane	Methylcyclopentane	nHeptane	Methylcyclohexane	n-Octane	1,1,1-Trichloroethane	Methyl Ethyl Ketone	[sopropano]	Trichloroethylene	Toluene	Ethlyene Dichloride	p-Xylene	m-Xylene	o-Xylene

Appendix V

Porton Gradicule Particle Sizing Data

Appendix V:

Porton Gradicule Particle Sizing of Dust Samples

Gradicule Calibration

Ernst Leitz Wetzler Binocular Microscope Eyepiece: 12.5x with Porton Gradicule

Object Lense: 10x

Porton	•	Micrometer crons calc	Log(d(i))
1		1.432	
2		2.086	
3		3.041	
4		4.431	
5		6.457	
6	8	9.410	0.903
7	15	13.71	1.176
8	21	19.98	1.322
9	31	29.12	1.491
10	44	42.43	1.643
11	62	61.84	1.792
12	89	90.12	1.949
13	123	131.3	2.089

Regression of Logarithm of Measured Diameter

Regression Output:

Constant	0
Std Err of Y Est	0.035
R Squared	0.992
No. of Observations	8
Degrees of Freedom	7

X Coefficient(s) 0.162 Std Err of Coef. 0.001

Appendix V: Stratified Data For Spray Painting

5 Minute Sampling Period

10% Object Lens

	10	0	0	0	0	0	0	0	0	C	
	တ	0	0	0	0	0	٥	0	0	0	0.00
	Φ	0	0	0	0	0	0	0	← 1	0	0.11 0.00
	~	0	0	₩.	0	ന	N	0	0	4	0.78
	9	ന	ന	S	2	₩	2	က	C)	#	2.44
	ហ	4	m		ო	ო	4	m	ហ	#	3.00
·	4	m	ហ	ហ	4	Q	ω	r ~-	Ø	m	5.56
Number	m	12	2	ហ	ω	12					7.80
Porton Number	8	ဖ	10	רט	16	16					10.60 7.80
_	ᆏ	10	~	16	17						12.50
	0										
	Field	Œ	8	ں	۵	Ш	Ŀ	9	I	Н	Ave per field

Count Frequency and Mass Frequency

Porton	d(i)) n(i)	ここの	Mass Cumm
	5		Freq Count (d(i))^3	Freq Mass
			Freq	Freq
₩.	0.716	12.50	0.292	
7	1.759	10.60	0.247 0.539 57.732	0.014 0.015
ന	2.563	7.80	0.722	
4	3.736	5.56	0.851	
ហ	5.444	3.00	0.922	
9	7.934	2.44	0.979	
7	11.56	0.78	0.997	
œ	16.84	0.11	7	0.135 1
Q	24.55	0.00	0	0
10	35.77	0.00		
11	52.14	0.00		
12	75.98	0.00		

3922.3

42.78

Total

Appendix V: Stratified Data For Spray Painting

10 Minute Sampling Period

10% Object Lens

	1 0	0	0	0	0	0	0	0	O	0	
,	თ	0	0	0	0	0	0	0	0	0	0.00
	Φ	0	0	0	0	-	0	0	0	0	0.11
	~	0	++	0	0	0	0	0	8	0	2.44 0.33
	Ø	+	e	4	4	m	m	T	e	0	2.44
	ហ	m	4	ľΩ	↔	~	٥	9	ω	ហ	5.00
	4	10	ω	רע	S	ញ	101	10	φ	~	8.89
Number	ო	ø	23	~	21	! !					
Jorton	73	13	9	7.5	4 Į						41.00 16.67 14.25
_	=-1	36	4	•							41.00
	0										eld
	Field	Œ	. a	ے د) <i>C</i>	ט נ	سا ل	ـ ب	ב כ		Ave per field

Count Frequency and Mass Frequency

	3884.3	88.69	Tata!
		Ö	12
		52.14 0.00	11
		Ö	10
		Ö	Ø
0.136	0.001 1 531.46	Ö	œ
	0.998	o.	٧
	0.994	Ċ	w
	0.967	ŭ,	IJ
	0.911	ω	4
	0.810	14.	ന
0.023 0.027	0.187 0.650 90.775	16.	ν.
600.0 500.0	Freq 0.462		₹1
Mass Cumm Freq Mass	Count Cumm n(i)* Freq Count (d(i))^3	d(i) n(i) Um	Porton

Appendix V: Stratified Data For Sanding

u ,	5 Minute Sampling Period	Sampl 1	ng F	Period	**	lox obj	10X Object Lens	กร					
		Port	ρί	Porton Number									
Field	0	-	N	m	4	ហ	Ø	۲-	œ	თ	1 0	- -	12
Œ					0	0	CJ	#	1	8	0	0	0
8					0	~	₩	0	-	0	0	0	0
ວ					0	0	2	4	⊣	0	₩	0	0
Q					0	⊣	7	₩.	0	0	-1	0	0
ш					1	2	7	2	0	-	0	0	0
ᄕ					0	-	2	2	2	-	0	0	0
9					0	m	4	ব	-	7	0	0	0
I					0	0	0	0	2	0	0	0	7
-					+	0	-	~	-	0	0		0
Ave													
per field	e ld			Ö	0.22	0.89	1.56	1.67	1.00	1.56 1.67 1.00 0.56	0.22 0.11 0.11	0.11	0.11

Count Frequency and Mass Frequency

Appendix V: Stratified Data For Sanding

	1	13	0	7	0	0	-	0	2	0	0		0.44
		12	+	0	0	0	0	0	7	7	m		0.78
		11	-	m	Ŋ	2	0	0	7	m	m		2.00 0
		10	₩	-	ന	ന	~	₩	7	7	7		1.78 2
		Ø	0	4	~	m	Ŋ	ເກ	m	ហ	m		4.67
10X Object Lens		Φ	4	4	2	ស	10	រប	Э	S	4		4.67
		~	Q	ស	ល	83	ſΩ.	۲-	Ø	10	4		95.9
		ဖ	12	9	9	~	10	2	8	9	~		7.67
		ហ	Ø	E	2	9	æ	m	រប	6	m		5.89
Ţ		4	ᆏ	m	ω	Ŋ	⊣	-	(T)	(1)	0		2.25
10 Minute Sampling Period	lumber	m	0	-	N	~	0	0	N	1	0		2
	Porton h	2	0	0	~		0	0	0	0	0		
	ď	- -1											
O Minu		0											РI
1.		Field	Œ	Φ.	ינו	0	ı Lul	L	. <u>ග</u>	I		A	per field

Count Frequency and Mass Frequency

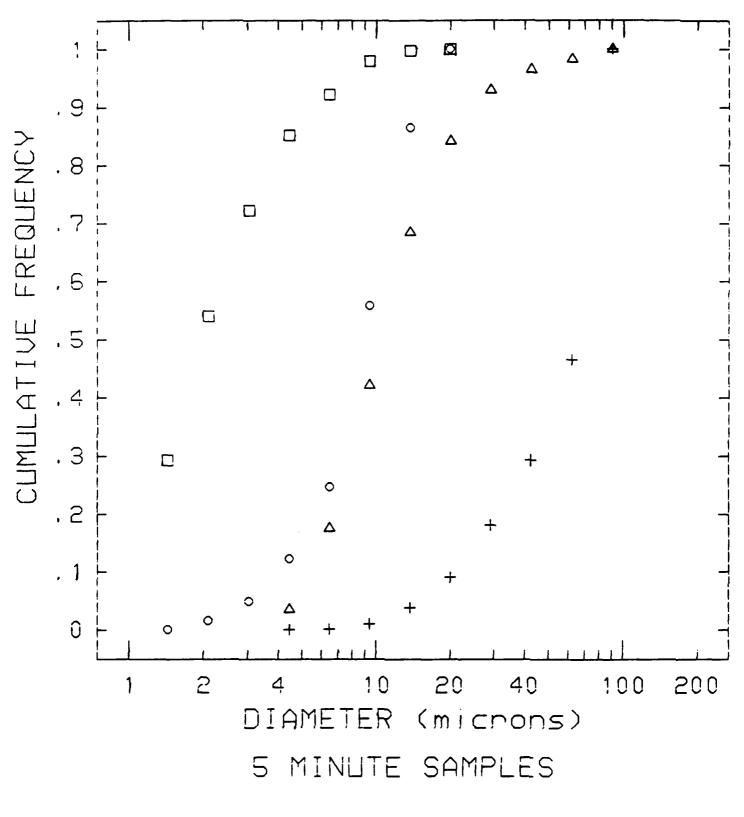
ĒΝΩ	0	0	0	0	8	m	0	9	ហ៍	32	32	ú	+
Cumm Mass Freq				000.0	0.00	0.00	0.01	0.05	0.0	0.13	0.33	0.573	
Mass Freq	0	0	0	0.000	0.000	0.002	0.007	0.015	0.048	0.057	0.200	0.240	0.426
n(i)* (d(i))^3	0	0	0	115,90	950.49	3829.3	10132.	22321.	69075.	81432.	283498	341174	908809
Count Freq		0	0	0.060	0.221	0.430	0.609	0.736	0.863	0.912	0.966	0.987	1
Count	0	0	0	090.0	0.160	0.209	0.178	0.127	0.127	0.048	0.054	0.021	0.012
n(i)	0.00	0.00	0.00	2.22	5.89	7.67	6.56	4.67	4.67	1.78	2.00	0.78	0.444
d(i) um	0.716	1,759	2.563	3,736	5.444	7.934	11.56	16.84	24.55	35.77	52.14	75.98	110.7
Porton	₩.	2	ო	4	ហ	9	2	œ	σ	10	11	12.	13

1E+06

36.66

Total

PAINTING & SANDING PARTICLE SIZES



- = PAINTING COUNT
 - PAINTING MASS
- A SANDING COUNT
- + SANDING MASS